

# Space-time QAM wireless MISO systems employing differentially coded in-/out-FECC SCQICs over slow-fading Jakes scattering mobile radio links

Ardavan Rahimian<sup>1</sup>, Farhad Mehran<sup>1</sup>, Robert G. Maunder<sup>2</sup>

<sup>1</sup>School of Electronic, Electrical and Computer Engineering, University of Birmingham, Birmingham B15 2TT, UK

<sup>2</sup>School of Electronics and Computer Science, University of Southampton, Southampton SO17 1BJ, UK

E-mail: rahimian@ieee.org

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**Abstract:** This study presents research that supplements and extends the previous works on design of space-time fully systematic unpunctured (FSU) serial concatenation of quadratic interleaved codes (SCQICs). The requirements for efficient design of the forward error correction (FEC) codecs motivated potential information-theoretic studies for enjoying the development of low-complex system components within the FEC encoder/decoder for securing the transmission reliability. Inspired by this motivation, this study not only provides design guidelines to achieve better bit error rate performance in terms of the major design factors of FSU-SCQICs, that is, component code constraint length and trellis structure, and FEC rate, but also estimates the gain gaps of different quadratic permutation (QP) structures in two crucial untouched aspects: (i) signal-to-noise ratio-region comparison on the optimality and (ii) investigation on the structural parameters of QPs, that is, cyclic shift and primitive factor.

## 1 Introduction

One of the most important design issues concerning research studies on the space-time turbo codes (STTCs) [1] aims to improve the key performance factors that have direct determinant effect on the overall bit error rate (BER) performance. Hence, it is vital to design the effective permutation arrays in regard to a waterfall-region of the BER curve and the region that exhibits a much shallower slope, that is, flare region. In particular, for the STTCs that enjoy cascaded systematic recursive convolutional codes (SRCCs) for yielding relatively high minimum distance, interleaver design issues are not reaching the state of maturity [2]. From theoretical design aspects, algebraic constructions are attracting particular interest for performing the scrambling/unscrambling functions since they yield provisioning coding gain in critical regions of the BER performance curve and enable possibility of analysis and compact representation. An additional enhancement which opens the way for their practical utilisation is their considerable lower implementation complexities.

## 2 Research contribution

It has been previously shown that serial turbo-like codes employing the quadratic permutations (QPs), that is, the serial concatenation of quadratic interleaved codes (SCQICs), result in outstanding coding gains [3–6]. This paper aims to supplement and extend the pivotal system design guidelines of our previous works in order to achieve a flexible SCQIC framework in terms of other crucial contradictory performance factors, so as to address the proposed SCQICs in co-operation with the highly matured technologies (e.g. bit-level space-time codes) employing the high-throughput modulation along with other specified features; which have been briefly outlined as follows:

- (1) *Component code structure:* Inspired by the motivation of finding promising generator polynomials which result in maximisation of component code minimum free distance [7]; this paper investigates the gain gap limits between provisioning choices of the convolutional component code (CCC) trellis structures for different feasible constraint lengths, with respect to the tolerable incurred decoding complexity, that is, the widely used range  $L \leq 5$ .
- (2) *FEC rate:* In terms of providing both coding gains and spectral efficiencies, flexible FEC code rate enables adaptation of provision

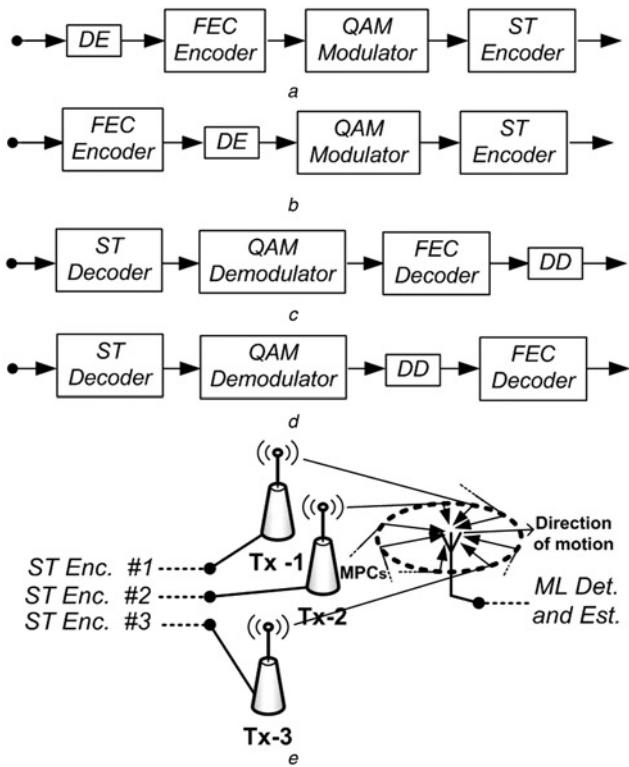
signal-to-noise ratio (SNR) operating point (which yields minimal BER) with respect to the bandwidth limitations of wireless channels. Hence, the investigation has been further broadened for lower code rates than typical 0.33, which is widely used for wireless transmissions.

- (3) *Differential coding (DC) inside-/outside-forward error correction codec (FECC):* There exist a wide range of advantages and disadvantages as a result of employing DC as the phase-ambiguity resolution technique [8] for high-throughput widely used 16-quadrature amplitude modulation (QAM) transmissions. One important issue of great theoretical and practical interest is to gain the benefits of DC technique while avoiding unnecessary BER degradation (because of the double-error phenomenon) by applying the DC external to the FECC, rather than modulating differentially coded version of FECC, that is, DC inside-FECC [9]. The studies (1) and (2) of this outlined list are supplemented by comparing the sacrificed gain gaps with respect to employing DC internal or external to FECC or the same system model based on the coherent detection.

- (4) *Optimality on SNR region(s):* Studies on comparison of different permutation algorithms to be employed in FEC-coded systems reveal that the superior BER performance of the selected one may yield inferior performance as interleaver size changes significantly. For example, for the parallel concatenated convolutional coding (PCCCing), although pseudo-random interleavers have been shown to have superior performance to the block interleavers for the large frame lengths, in many cases their inferior performance in the low frame sizes has been confirmed [10]. Hence, the inevitable investigation for the gain gaps between SCQICs with respect to reference of comparison, that is, the same system using randomly generated scramblers/unscramblers, are carried out in order to ensure that the gap is not significant; i.e. not yielding unexpected high probability of bit error and hence changing the unexpected level of optimality in particular SNR region.

- (5) *Structural parameters of QPs:* Monte Carlo computer simulations have been conducted in order to potentially predict the performance of SCQICing when the QP-vectors utilise different multiplicative factors and cycle shifts.

The system investigations have been thoroughly conducted in a rich isotropic scattering mobile radio channel based on the Jakes



**Fig. 1** STTC encoder/decoder  
*a* External-FECC-DC SCQIC encoder  
*b* Internal-FECC-DC SCQIC encoder  
*c* DD-out-FECC iterative SCQIC decoder  
*d* DD-in-FECC iterative SCQIC decoder  
*e* Conceptual representation of Jakes scattering wireless MISO mobile radio link

Doppler power spectrum [11]; that is, where a scatter ring is placed around the receiver in order to model and analyse the multipath components, and the isotropic continuum of arriving components is approximated by the plane radiowaves arriving at the uniformly spaced azimuthal angles.

### 3 Wireless system model

#### 3.1 STTC encoder/decoder

Fig. 1 outlines the wireless system architecture operating in portrayed conceptual representation of uniformly distributed scattering. For the DC outside-FECC scheme, that is, Fig. 1*a*, the differential encoder (DE) is fed with a  $(N/2)$ -bit information frame  $u = (u_0, \dots, u_k)$  based on the Bernoulli distribution, with the pmf  $f(k, p) = p$  if  $k = 1, (1 - p)$  if  $k = 0$ , and 0 otherwise. The outer SRCC encoder is fed by either of the DC-coded bit stream (for the case of external DC) or information frame for coherent and internal DC-based systems. The selected half-rate outer SRCC trellis structures for  $r \leq 0.33$  and  $L \leq 5$  are tabulated in Table 1. The interleaver applies the QP on the bit sequences obtained from the previous step, which is originally proposed in [12, 13] and further developed for serial turbo-like codes in [3–6]. Let  $x_{oc} = (x_0, \dots, x_{N-1})$  be a sequence in  $\{0, 1\}^N$  which is the  $N$ -bit outer system coded sequence. The QP-based interleaver maps the  $x_{oc}$  to a sequence  $\hat{x}_{oc} = (x_0, \dots, x_{N-1})$  according to Theorems I and II of [12] (examples are given in the next section). The inner SRCC encoder is fed with  $\hat{x}_{oc}$ , that is, an  $N$ -bit block containing the QP-permutation sequence of outer coded bit stream. The selected inner SRCC trellis structures with  $r^i \in \{0.66, 0.5, 0.4\}$  for  $r \leq 0.33$  and  $L \leq 5$  are tabulated in Table 1. For the DC inside-FECC scheme, that is, Fig. 1*b*, the DE is fed with a  $(N/r^o)$ -bit SCQIC-coded sequence. Compared with this scheme, the major advantage of using the DC external to the FECC is that the double-error phenomenon because of the consecutive errors has been eliminated. However, since the system resolution performance depends on the synchroniser circuit of the channel decoder, applying the DC outside FECC is not appropriate for the application to burst mode [9]. The resultant SCQIC can readily be applied to 16-QAM modulation in order to provide a good solution in terms of both power and bandwidth efficiencies. Meanwhile, the low-operating SNR of the resultant STTC increases the transmission robustness to interference and distortion. The QAM modulator maps the DC-SCQICs of  $(N/r^o)$ -bit blocks to the symbol  $\mathfrak{S}_k$  from the  $2^Q$ -ary constellation set  $S = \{\alpha_1, \alpha_2, \dots, \alpha_{2^Q}\}$ , where  $\alpha_i$  corresponds to the bit pattern  $s_i = [s_{i,1}, s_{i,2}, \dots, s_{i,Q}]$  with  $s_{i,j} \in \{0, 1\}$ . Space-time encoding process follows the wireless transmission sequences for the triplet-antenna systems derived in (37) of [14].

**Table 1** CCC structures

Constraint length, $L$	Overall rate, $r$	Outer trellis structure and rate, $r^o = 1/2$	Inner trellis structure and rate, $r^i$
3	1/3	$G_3^o: \{111, 101\}_2$	$r^i = 2/3 \quad G_3^i: \left\{ \begin{matrix} 111, 101, 000; \\ 000, 111, 101 \end{matrix} \right\}_2$
	1/4	same as $G_3^o$	$r^i = 2/4 \quad G_3^i: \left\{ \begin{matrix} 111, 101, 011, 000; \\ 000, 111, 101, 011 \end{matrix} \right\}_2$
	1/5	same as $G_3^o$	$r^i = 2/5 \quad G_3^i: \left\{ \begin{matrix} 111, 101, 011, 010, 000; \\ 000, 111, 101, 011, 010 \end{matrix} \right\}_2$
4	1/3	$G_4^o: \{1111, 1101\}_2$	$r^i = 2/3 \quad G_4^i: \left\{ \begin{matrix} 1111, 1101, 000; \\ 000, 1111, 1101 \end{matrix} \right\}_2$
	1/4	same as $G_4^o$	$r^i = 2/4 \quad G_4^i: \left\{ \begin{matrix} 1111, 1101, 1011, 000; \\ 000, 1111, 1101, 1011 \end{matrix} \right\}_2$
	1/5	same as $G_4^o$	$r^i = 2/5 \quad G_4^i: \left\{ \begin{matrix} 1111, 1101, 1011, 1001, 000; \\ 000, 1111, 1101, 1011, 1001 \end{matrix} \right\}_2$
5	1/3	$G_5^o: \{11111, 10001\}_2$	$r^i = 2/3 \quad G_5^i: \left\{ \begin{matrix} 11111, 10001, 00000; \\ 00000, 11111, 10001 \end{matrix} \right\}_2$
	1/4	same as $G_5^o$	$r^i = 2/4 \quad G_5^i: \left\{ \begin{matrix} 11111, 10001, 10011, 00000; \\ 00000, 11111, 10001, 10011 \end{matrix} \right\}_2$
	1/5	same as $G_5^o$	$r^i = 2/5 \quad G_5^i: \left\{ \begin{matrix} 11111, 10001, 10011, 10111, 00000; \\ 00000, 11111, 10001, 10011, 10111 \end{matrix} \right\}_2$

At the receiver, for detecting symbols of the system, the maximum-likelihood (ML) detector amounts to minimise the decision metrics given in [15], and the resultant sequences are inserted in demodulator block. At the demodulator, the QAM constellations are demapped in order to form the system blocks of SCQIC-coded bit stream, that is, demaps the symbol  $\hat{s}_k$  from the  $2^Q$ -ary constellation set  $S$  to DC-SCQICs of  $(N/r^Q)$ -bit blocks. For the case of the DC internal to FECC, the detected symbols are inserted into the differential decoder (DD) for applying the inverse function of DE, whereas for DC external to FECC the input to the DD is the iteratively decoded SCQIC bit sequences. The demodulator's output has also been computed based on the hard-decision. The system channel values (i.e. soft-decision log-likelihood ratios (LLRs)) have been computed by a separate function at the FEC decoder at the initialisation step of the system iterative decoding.

The DD bit stream inserted into the system SCQIC decoder for recovering the transmitted bits follows near-ML iterative decoding procedure developed for the SCQICs in [6]. Herein, constituent decoders corresponding to SRCC trellis structures iteratively exchange extrinsic information between themselves at the core of the SCQIC iterative decoder architecture. The targeted investigations have been systematically carried out based on the Log-maximum a posteriori (MAP) decoders [8], but the effects of using other decoders for SCQICs are addressed in [6]. For necessary deinterleaving at the decoder architecture, the re-arranged QP feature will be more exploited in Section 4; wherein the samples of the bit streams are scrambled and unscrambled.

### 3.2 Wireless system specifications

We assume rich scattering environments where the receiver antenna responds to each transmitter antenna system through a statistically independent fading coefficient [16], given the wireless transmission is performed using the Gray-coded (GC)-16-QAM. The selected set of the trellis structures for  $L \leq 5$  are tabulated in Table 1, supplemented by all extended variants for the FEC rates 1/3, 1/4 and 1/5, that is, every source data bit (or DE data bit in out-DC-FECC) is mapped into three, four and five symbols, respectively. We assume that both the outer and inner SRCCs are terminated by  $L - 1$  tail bits in order to drive the encoders to all-zero state. For the half-rate space-time coded system, the measured Doppler spectrum of targeted isotropic scattering mobile radio channel is compared with theoretical Jakes spectrum as in Fig. 2. The signal amplitude received by Rx is affected by the presence of slow-fading Rayleigh flat-fading mechanism and corrupted by additive noise, and follows the channel matrix descriptions as in [2]. The channel modelling analysis has employed the stochastic system models, and considers the generic probability density function (PDF) of the field strength in the intended wireless link. Therefore, the bandlimited impulse response for the three slow-fading links is depicted in Fig. 3, in order to clearly demonstrate

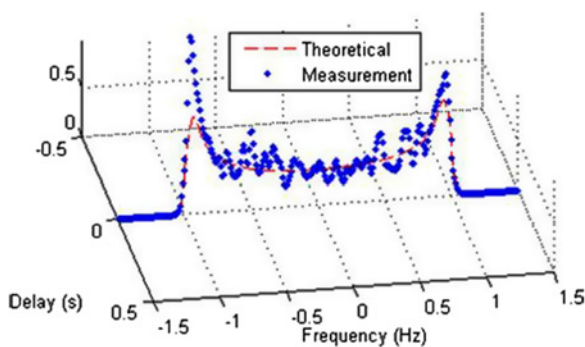


Fig. 2 Computed theoretical against measured Jakes Doppler spectra of a path against path delay(s) in one branch of wireless MISO mobile radio link

the link's impulse response in the proposed analytical case of  $3 \times 1$  links along with the given specifications without affecting the overall system BER performance. It is also assumed that the stationary scatterers are on average distributed uniformly on a circle around the receiver with omnidirectional antenna, with the same average power from all directions. Invoking the central limit theorem, we can assume that power from one direction is complex Gaussian distributed. In addition, the technical issues related to the intended stochastic multiple antenna channel modelling tackles the same procedure as given in [2, 6].

If we assume that the receiver moves with a certain speed, the number of components coming from each direction will take the tub form of Jakes spectrums, given analytically by  $S_D(v) = (1/\pi \cdot v_{\max}) \cdot (1 - (v/v_{\max})^2)^{-1/2}$  for  $-v_{\max} \leq v \leq v_{\max}$  [17], where  $f_{\max}$  is the maximum Doppler-shift. The scatterers are equally distributed in all directions and the receiver is also moving. The radio signal from all directions has on average the same power and delay. The spectrum can be interpreted such that infinite contributions, which are very small, come from 0 and 180°, which creates two singularities in  $v_{\max}$  and  $-v_{\max}$ .

## 4 Numerical results and discussion

In this section, representative wireless system performance evaluation results have been used in order to characterise the attainable

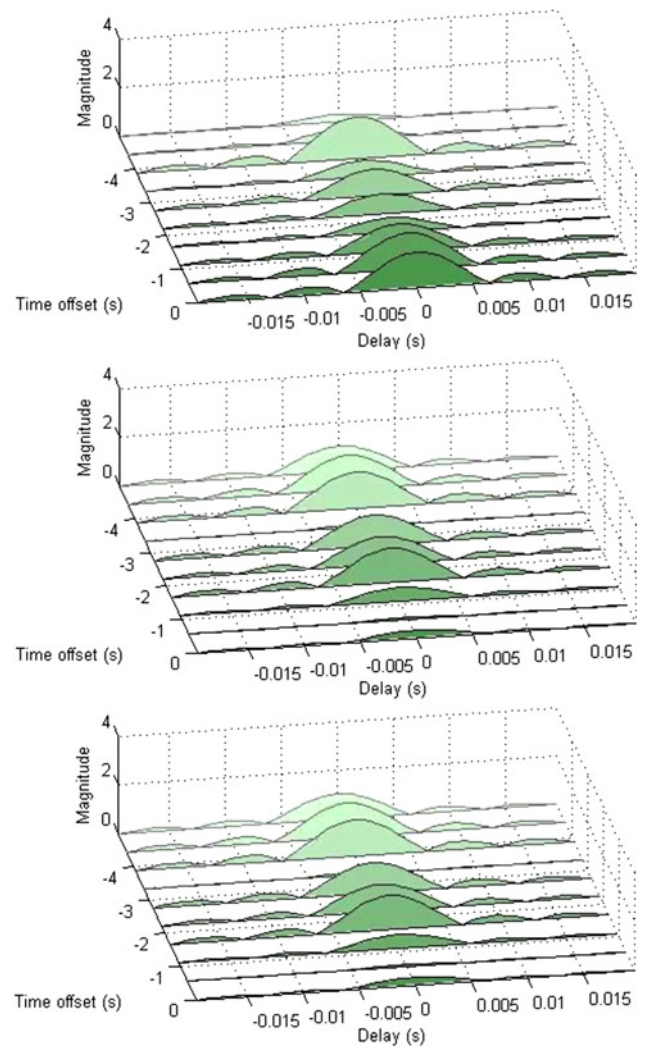


Fig. 3 Snapshots of computed bandlimited impulse response for the three slow-fading quasi-static wireless MISO mobile radio links; the darkest curve presenting the current response at BER =  $1.778e - 4$  and  $E_b/N_0 = 4$  dB

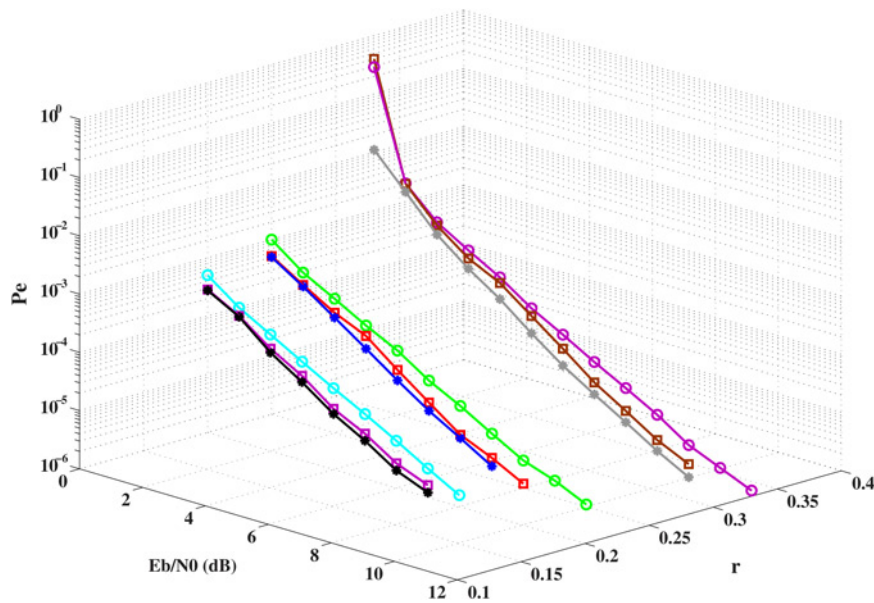


Fig. 4 Comparison of BER against  $E_b/N_0$  against  $r$  for the coherent wireless systems

performance of the coded multiple-input-single-output (MISO) systems from the aspects outlined in Section 1. In Figs. 4–6, the BER is shown against the energy per bit/noise power spectral density ( $E_b/N_0$ ) and the FEC rate ( $r$ ) for coherent, out-FECC DC and in-FECC DC systems. Herein, the lines with circle, square and star markers present the performance curves associated with employing  $L=3, 4$  and  $5$ . The particular generator polynomials are chosen so that the designed SCQIC does not have catastrophic error propagation and has high free distance for the selected FEC rates and the constraint lengths. Meanwhile, FEC rates and component code constraint lengths are chosen from among the most widely used range for provisioning overall design tradeoff. As it can be seen, the huge difference in performance that can result from extra parity bit as a result of lowering FEC rate is on average of 2 dB when the comparison is made for fixed-length CCCs with the same trellis structure.

For  $r=1/3 \rightarrow 1/5$  coding gains of up to  $\approx 4$  dB are achieved at the expense of spectral efficiency degradations because of two extra parity bits.

The performance improvement due to employing the CCCs with the higher  $L$  becomes not outstandingly significant, and suggests to limit the  $L < 6$  in order to avoid the considerable increase in system decoding complexities which does not result in worthwhile BER reduction, neither in waterfall-region, nor in flare region; that is, based on [8], increasing the  $L$  by a factor one (e.g.  $L: 3 \rightarrow 4$  or  $L: 4 \rightarrow 5$ ) requires around two times more additions, multiplications and maximisation operations when Max-Log-MAP algorithm is employed at the iterative decoder, while yield performance gains around 1 dB according to Figs. 4–6 for attaining  $BER \approx 10^{-6}$ . As far as the Log-MAP algorithm is a more interesting candidate to be used for yielding performance close to original MAP decoders by using correction function, the number of lookups required for

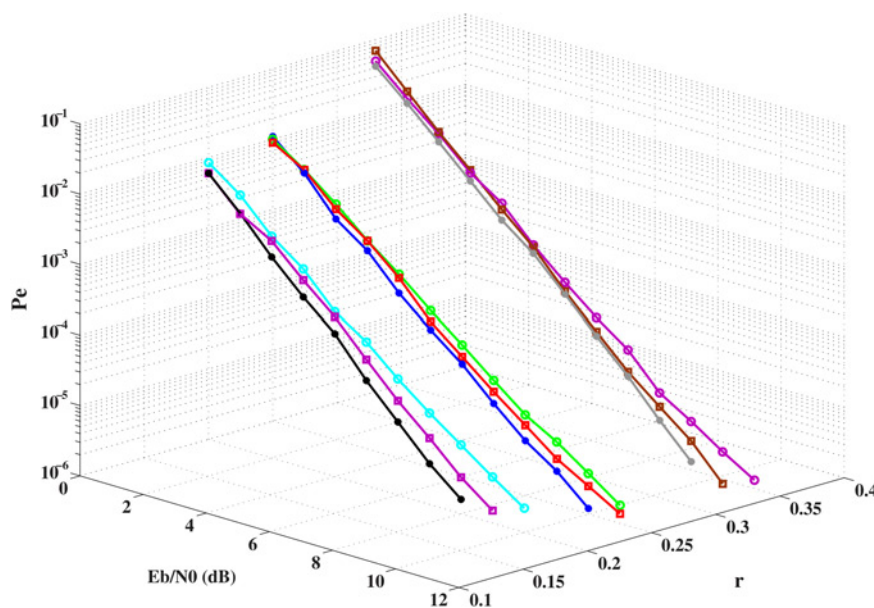


Fig. 5 Comparison of BER against  $E_b/N_0$  against  $r$  for the wireless system with out-DC-FECC

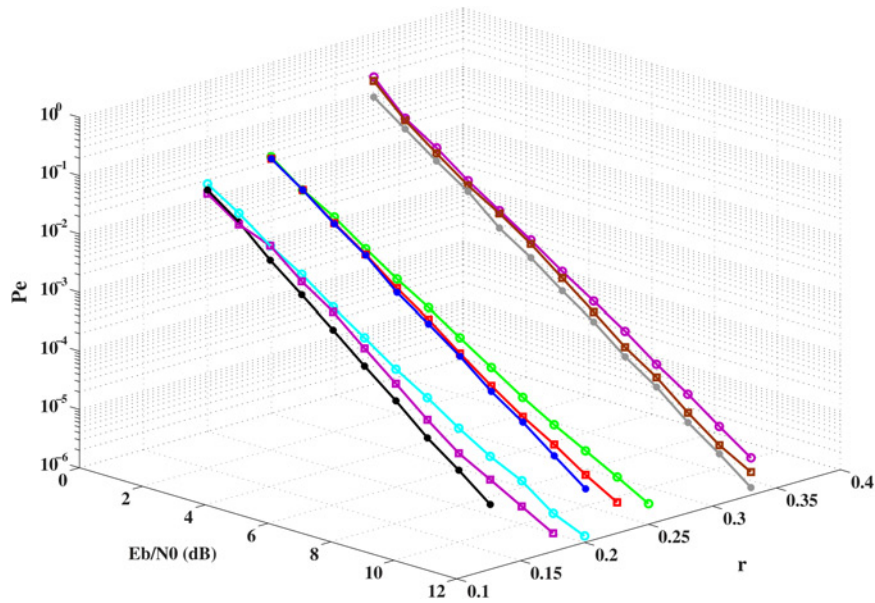


Fig. 6 Comparison of BER against  $E_b/N_0$  against  $r$  for the wireless system with in-DC-FECC

computing correction function brings further operations for the practical use of high constraint lengths.

As be seen from the performance curves, since for DC-in-FECC one erroneously detected phase will cause two successive false symbols even if the next phase is received correctly, that is, double-error phenomenon, the error burst causes serious BER degradation of above 2 dB compared with the coherent systems. For reducing the highly correlated errors, in DC-out-FECC scheme, the SCQIC decoder does not encounter the double-error phenomenon and only the BER of SCQIC decoder output is doubled. Hence, doubling the SCQIC decoder BER yields a smaller coding gain loss at the expense of using synchroniser circuit for SCQIC decoder, which is not suitable for applications where long delay for resolving the phase ambiguity cannot be tolerated [9].

The effects of changing the structure of the QP-vectors and their lengths have been examined in this part. For instance, according to design Theorems I and II of [12], the QP-vectors for  $N=16$  and 32 are given as follows, where  $\pi_N^{(C,F)}$  denotes the vector associated with QP-length  $N$ , with cyclic shift  $C$  and multiplicative factor  $F$  (see equation at the bottom of the next page).

Hence, for instances of 16-/32-bit permutation lengths, the QP-based interleaver maps generated sequences from half-rate outer SRCC trellis structures for  $r \leq 0.33$  and  $L \leq 5$ , for example

$$\begin{aligned} \rightarrow \bar{v} &= \langle 1110001010011000 \rangle_{16} \\ \rightarrow \bar{v} &= \langle 11100010100110001110001010011000 \rangle_{32} \end{aligned}$$

Into the reordered sequences of  $w_C^F$  given as follows:

For  $\pi_{16}$  (see equation at the bottom of next page)

For  $\pi_{32}$

(see equation at the bottom of next page)

For the case of message passing between the component decoders corresponding to outer/inner SRCC trellis structures, the input of outer decoder from the output of inner decoder utilises the inverse of this function at the deinterleaver. Instances of the QP-based deinterleaving are given as follows, where the  $\tilde{w}_C^F$  is an

$$\pi_N^{(C,F)} \left\{ \begin{array}{l} \pi_{16} : \left\{ \begin{array}{l} \pi^{1,F \in \{1:15\}_{\text{odd}}} : \left\{ \begin{array}{l} \pi^{1,1} = [4, 15, 7, 14, 13, 11, 3, 1, 9, 16, 10, 5, 8, 12, 6, 2] \\ \dots \\ \pi^{1,15} = [12, 6, 10, 13, 8, 2, 9, 1, 15, 7, 5, 4, 11, 3, 14, 16] \\ \dots \end{array} \right. \\ \pi^{15,F \in \{1:15\}_{\text{odd}}} : \left\{ \begin{array}{l} \pi^{15,1} = [6, 2, 4, 15, 7, 14, 13, 11, 3, 1, 9, 16, 10, 5, 8, 12] \\ \dots \\ \pi^{15,15} = [14, 16, 12, 6, 10, 13, 8, 2, 9, 1, 15, 7, 5, 4, 11, 3] \end{array} \right. \\ \pi_{32} : \left\{ \begin{array}{l} \pi^{1,F \in \{1:31\}_{\text{odd}}} : \left\{ \begin{array}{l} \pi^{1,1} = [4, 15, 7, 14, 32, 11, 30, 26, 25, 16, 31, 6, 24, 28, 22, 1, 17, 8, 18, 13, 29, 20, \\ \quad 3, 9, 12, 23, 10, 5, 21, 19, 27, 2] \\ \dots \\ \pi^{1,31} = [7, 15, 13, 29, 24, 11, 22, 25, 31, 14, 5, 21, 16, 26, 17, 1, 12, 6, 10, 28, 3, 18, \\ \quad 9, 8, 4, 23, 2, 20, 27, 19, 30, 32] \\ \dots \end{array} \right. \\ \pi^{31,F \in \{1:31\}_{\text{odd}}} : \left\{ \begin{array}{l} \pi^{31,1} = [27, 2, 4, 15, 7, 14, 32, 11, 30, 26, 25, 16, 31, 6, 24, 28, 22, 1, 17, 8, 18, 13, 29, \\ \quad 20, 3, 9, 12, 23, 10, 5, 21, 19] \\ \dots \\ \pi^{31,31} = [30, 32, 7, 15, 13, 29, 24, 11, 22, 25, 31, 14, 5, 21, 16, 26, 17, 1, 12, 6, 10, 28, \\ \quad 3, 18, 9, 8, 4, 23, 2, 20, 27, 19] \end{array} \right. \end{array} \right. \end{array} \right.$$

arbitrary sequence

$$\begin{aligned} \tilde{w}_5^5 &= \langle 1110001010011000 \rangle_{16} \xrightarrow{\pi^{-1}} \langle 0001010111000101 \rangle_{16} \\ \tilde{w}_{21}^2 &= \langle 11100010100110001010001010010101 \rangle_{32} \\ &\xrightarrow{\pi^{-1}} \langle 1010100100000001100011011110101 \rangle_{32} \end{aligned}$$

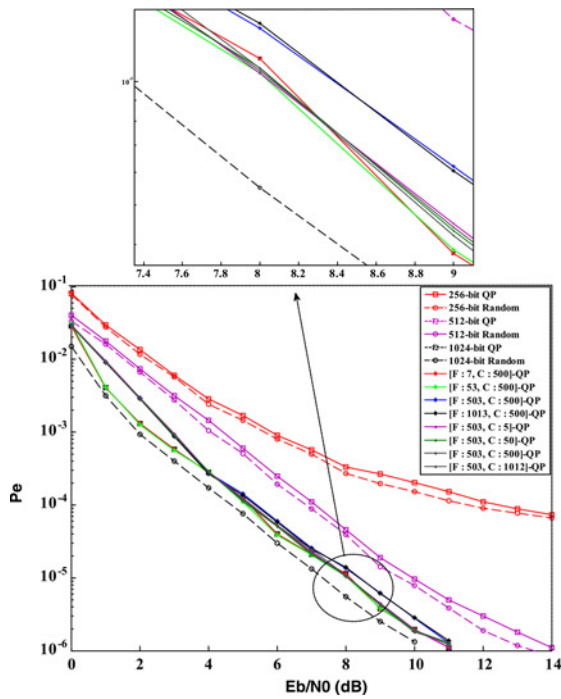
As it has been shown, for the case of permutations with different  $F$ s and  $C$ s, different randomisation mappings can be constructed. In Fig. 7, these variations have been investigated for the high gain

$N = 1024$  system, where the  $F$  and  $C$  are chosen in mid-range of different size categories. So, when either of  $F$  or  $C$  is varying, the other is fixed to its mid-range value. As it can be seen, as far as the gain gaps are negligible, the selection of structural parameters for construction of QPs makes no significant BER superiority/inferiority.

In the classic turbo coding and its subsequent contributions, exceptional coding gains have been reported to be attained in the case of employing long permutations, that is,  $N$  exceeds 10 000 bits such as, for example, Berrou's classic half-rate PCCCing with  $N = 65\,536$  bits. However, since the extra complexity and delay are not just

$$w_{1:15}^1 \cdot \left\{ \begin{array}{l} \langle 0010101110000101 \rangle \\ \langle 0101011100001010 \rangle \\ \langle 1010111000010100 \rangle \\ \langle 0101110000101001 \rangle \\ \langle 1011100001010010 \rangle \\ \langle 0111000010100101 \rangle \\ \langle 1110000101001010 \rangle \\ \langle 1100001010010101 \rangle \\ \langle 1000010100101011 \rangle \\ \langle 0000101001010111 \rangle \\ \langle 0001010010101110 \rangle \\ \langle 0010100101011100 \rangle \\ \langle 0101001010111000 \rangle \\ \langle 1010010101110000 \rangle \\ \langle 0100101011100001 \rangle \end{array} \right\} \dots w_{1:15}^5 \cdot \left\{ \begin{array}{l} \langle 0101000111001100 \rangle \\ \langle 1010001110011000 \rangle \\ \langle 0100011100110001 \rangle \\ \langle 1000111001100010 \rangle \\ \langle 0001110011000101 \rangle \\ \langle 0011100110001010 \rangle \\ \langle 0111001100010100 \rangle \\ \langle 1110011000101000 \rangle \\ \langle 1100110001010001 \rangle \\ \langle 1001100010100011 \rangle \\ \langle 0011000101000111 \rangle \\ \langle 0110001010001110 \rangle \\ \langle 1100010100011100 \rangle \\ \langle 100010100011100 \rangle \\ \langle 000101000111001 \rangle \end{array} \right\} \dots w_{1:15}^{15} \cdot \left\{ \begin{array}{l} \langle 1001011101000100 \rangle \\ \langle 0010111010001001 \rangle \\ \langle 0101110100010010 \rangle \\ \langle 1011101000100100 \rangle \\ \langle 0111010001001001 \rangle \\ \langle 1110100010010010 \rangle \\ \langle 1101000100100101 \rangle \\ \langle 1010001001001011 \rangle \\ \langle 0100010010010111 \rangle \\ \langle 1000100100101110 \rangle \\ \langle 0001001001011101 \rangle \\ \langle 0010010010111010 \rangle \\ \langle 0100100101110100 \rangle \\ \langle 1001001011101000 \rangle \\ \langle 0010010111010001 \rangle \end{array} \right\}$$

$$w_{1:31}^1 \cdot \left\{ \begin{array}{l} \langle 00100000100001011011101111000101 \rangle \\ \langle 01000001000010110111011110001010 \rangle \\ \langle 10000010000101101110111100010100 \rangle \\ \langle 00000100001011011101111000101001 \rangle \\ \langle 00001000010110111011110001010010 \rangle \\ \langle 00010000101101110111100010100100 \rangle \\ \langle 00100001011011101111000101001000 \rangle \\ \langle 01000010110111011110001010010000 \rangle \\ \langle 10000101101110111100010100100000 \rangle \\ \langle 00001011011101111000101001000001 \rangle \\ \langle 00010110111011110001010010000010 \rangle \\ \langle 00101101110111100010100100000100 \rangle \\ \langle 01011011101111000101001000001000 \rangle \\ \langle 10110111011110001010010000010000 \rangle \\ \langle 01101110111100010100100000100001 \rangle \\ \langle 11011101111000101001000001000010 \rangle \\ \langle 10111011110001010010000010000101 \rangle \\ \langle 01110111100010100100000100001011 \rangle \\ \langle 1101111000101001000001000010110 \rangle \\ \langle 1110111000101001000001000010110 \rangle \\ \langle 11011110001010010000010000101101 \rangle \\ \langle 10111100010100100000100001011011 \rangle \\ \langle 01111000101001000001000010110111 \rangle \\ \langle 11110001010010000010000101101110 \rangle \\ \langle 11100010100100000100001011011101 \rangle \\ \langle 11000101001000001000010110111011 \rangle \\ \langle 10001010010000010000101101110111 \rangle \\ \langle 00010100100000100001011011101111 \rangle \\ \langle 00101001000001000010110111011110 \rangle \\ \langle 01010010000010000101101110111100 \rangle \\ \langle 1010010000010000101101110111000 \rangle \\ \langle 0100100000100001011011101110001 \rangle \end{array} \right\} \dots w_{1:31}^{11} \cdot \left\{ \begin{array}{l} \langle 10100001011000011101000000101111 \rangle \\ \langle 01000010110000111010000001011111 \rangle \\ \langle 10000101100001110100000010111110 \rangle \\ \langle 00001011000011101000000101111101 \rangle \\ \langle 00010110000111010000001011110101 \rangle \\ \langle 00101100001110100000010111110100 \rangle \\ \langle 01011000011101000000101111101000 \rangle \\ \langle 10110000111010000001011111010000 \rangle \\ \langle 01100001110100000010111110100001 \rangle \\ \langle 11000011101000000101111101000010 \rangle \\ \langle 10000111010000001011111010000101 \rangle \\ \langle 00001110100000010111110100001011 \rangle \\ \langle 00011101000000101111101000010110 \rangle \\ \langle 00111010000001011111010000101100 \rangle \\ \langle 01110100000010111110100001011000 \rangle \\ \langle 11101000000101111101000010110000 \rangle \\ \langle 11010000001011111010000101100001 \rangle \\ \langle 10100000010111110100001011000011 \rangle \\ \langle 01000000101111101000010110000111 \rangle \\ \langle 10000001011111010000101100001110 \rangle \\ \langle 00000010111110100001011000011101 \rangle \\ \langle 00000101111101000010110000111010 \rangle \\ \langle 00001011111010000101100001110100 \rangle \\ \langle 00101111101000010110000111010000 \rangle \\ \langle 01011111010000101100001110100000 \rangle \\ \langle 10111110100001011000011101000000 \rangle \\ \langle 01111101000010110000111010000001 \rangle \\ \langle 11111010000101100001110100000010 \rangle \\ \langle 11110100001011000011101000000101 \rangle \\ \langle 11101000010110000111010000001011 \rangle \end{array} \right\}$$



**Fig. 7** Comparison of BER curves for QP-/random-based interleaved wireless systems with  $200 \simeq N \simeq <1000$ ; comparison of gain gaps between QP-based systems for selected cycle shifts ( $C_s$ ) and multiplicative factors ( $F_s$ )

tified for modern wireless applications, the fundamental design issues of channel codes directed a great deal of efforts for designing short-length FECs; that is, adopting short-frame system structures at expense of BER degradations. Hence, this design guideline limits our investigation to be conducted for range  $N \simeq <1000$  bits; that is, for the comparative investigation between the QP and the random permutations' gain gaps for different lengths because of the reason discussed in (4) of the outlined list in Section 2. Fig. 7 further shows the performance curves as a function of interleaver size, which presents how performance improves as the interleaver length increases for  $N_{INT} \simeq <1000$ . The following important observations can be made from the obtained results: (i) As far as the QP- and random-based systems are operating in close SNRs, that is, gain gaps for yielding similar BER are not high for the three possible interleaver lengths in  $200 \simeq N \simeq <1000$  range (i.e.  $N \in \{256, 512, 1024\}$ ) the research suggests to employ QPs for modern short-frame applications which also require lower implementation complexities. (ii) For the three possible and selected  $N_s$  which satisfy both QP construction conditions and  $N \simeq <1000$ , 256 bit scheme is not capable of operating without an error floor. Whereas the 512 bit scheme is provisioning the BER performance in both waterfall and flare regions, and reduces the further complexities associated with the high gain  $N = 1024$  bit scheme.

## 5 Conclusion

In this paper, in order to contrive an attractive design tradeoff for the QP-based STTCs, algebraic permutation and SRCC component code design issues and FEC-rate flexibility, which have dramatic

$\cdot w_{1:31}^{21} \cdot$	$\langle 00011010111000010111000110001100 \rangle$ $\langle 00110101110000101110001100011000 \rangle$ $\langle 01101011100001011100011000110000 \rangle$ $\langle 11010111000010111000110001100000 \rangle$ $\langle 10101110000101110001100011000001 \rangle$ $\langle 01011100001011100011000110000011 \rangle$ $\langle 10111000010111000110001100000110 \rangle$ $\langle 01110000101110001100011000001101 \rangle$ $\langle 11100001011100011000110000011010 \rangle$ $\langle 11000010111000110001100000110101 \rangle$ $\langle 10000101110001100011000001101011 \rangle$ $\langle 00001011100011000110000011010111 \rangle$ $\langle 00010111000110001100000110101110 \rangle$ $\langle 00101110001100011000001101011100 \rangle$ $\langle 01011100011000110000011010111000 \rangle$ $\langle 10111000110001100000110101110000 \rangle$ $\langle 01110001100011000001101011100001 \rangle$ $\langle 11100011000110000011010111000010 \rangle$ $\langle 11000110001100000110101110000101 \rangle$ $\langle 10001100011000001101011100001011 \rangle$ $\langle 00011000110000011010111000010111 \rangle$ $\langle 00110001100000110101110000101110 \rangle$ $\langle 01100011000001101011100001011100 \rangle$ $\langle 11000110000011010111000010111000 \rangle$ $\langle 10001100000110101110000101110001 \rangle$ $\langle 00011000001101011100001011100011 \rangle$ $\langle 00110000011010111000010111000110 \rangle$ $\langle 01100000110101110000101110001100 \rangle$ $\langle 11000001101011100001011100011000 \rangle$ $\langle 10000011010111000010111000110001 \rangle$ $\langle 00011000001101011100001011100011 \rangle$ $\langle 00110000011010111000010111000110 \rangle$ $\langle 01100000110101110000101110001100 \rangle$ $\langle 11000001101011100001011100011000 \rangle$ $\langle 10000011010111000010111000110001 \rangle$ $\langle 00000110101110000101110001100011 \rangle$	$\dots \cdot w_{1:31}^{31} \cdot$	$\langle 10110001000000111001111001100100 \rangle$ $\langle 01100010000001110011110011001001 \rangle$ $\langle 11000100000011100111100110010010 \rangle$ $\langle 10001000000111001111001100100101 \rangle$ $\langle 00010000001110011110011001001011 \rangle$ $\langle 00100000011100111100110010010110 \rangle$ $\langle 01000000111001111001100100101100 \rangle$ $\langle 10000001110011110011001001011000 \rangle$ $\langle 00000011100111100110010010110001 \rangle$ $\langle 00000111001111001100100101100010 \rangle$ $\langle 00001110011110011001001011000100 \rangle$ $\langle 00011100111100110010010110001000 \rangle$ $\langle 00111001111001100100101100010000 \rangle$ $\langle 01110011110011001001011000100000 \rangle$ $\langle 11100111100110010010110001000000 \rangle$ $\langle 11001111001100100101100010000001 \rangle$ $\langle 10011110011001001011000100000011 \rangle$ $\langle 00111100110010010110001000000111 \rangle$ $\langle 01111001100100101100010000001110 \rangle$ $\langle 11110011001001011000100000011100 \rangle$ $\langle 11100110010010110001000000111001 \rangle$ $\langle 11001100100101100010000001110011 \rangle$ $\langle 10011001001011000100000011100111 \rangle$ $\langle 00110010010110001000000111001111 \rangle$ $\langle 01100100101100010000001110011110 \rangle$ $\langle 11001001011000100000011100111100 \rangle$ $\langle 10010010110001000000111001111001 \rangle$ $\langle 00100101100010000001110011110011 \rangle$ $\langle 01001011000100000011100111100110 \rangle$ $\langle 10010110001000000111001111001100 \rangle$ $\langle 00101100010000001110011110011001 \rangle$
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effect on the free distance of the resultant STTC method, have been all addressed and characterised when they are all amalgamated. The results of this paper can be extended in a number of ways which are of great theoretical and practical interest, including investigation on the potential enhancements as a result of deploying directional antennas at one or both ends of the MISO radio link, and investigation over mobile-to-mobile scattering propagation environments.

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