

# Unprecedented Electromagnetic Shielding Effectiveness of Lightweight Nonwoven Ag/PA66 Fabrics

Ozen M.S.<sup>1,2</sup>, Sancak E.\*<sup>1,2</sup>, Soin N.<sup>2</sup>, Shah T.H.<sup>2</sup>, Zarei A<sup>2</sup>, Siores E.<sup>2</sup>

<sup>1</sup>Marmara University, Technology Faculty, Department of Textile Engineering, Istanbul, TURKEY.

<sup>2</sup>Institute for Materials Research and Innovation (IMRI), University of Bolton, Bolton, UK.

\*Corresponding Author: [esancak@marmara.edu.tr](mailto:esancak@marmara.edu.tr)

## Abstract

Novel, high-performance silver coated polyamide, Ag/PA66, nonwoven fabrics with a density of only 0.04g/cm<sup>3</sup> have been developed using staple fibres of 19 (3.3dtex) and 27 (6.7dtex) µm diameter. The obtained nonwoven fabrics with an Ag loading of 12-18wt% exhibited excellent weight-normalised specific electromagnetic shielding effectiveness of over 1200 dB/(g/cm<sup>3</sup>) in the 0.015-3GHz range, which is among the highest reported till date. Moreover, the applied microwave was verified to be absorbed rather than being reflected back making the fabrics highly suitable for shielding applications. It was also observed that nonwoven fabrics made from finer 3.3dtex Ag/PA66 fibres have higher reflection and lower absorption values than their thicker (6.7dtex) counterparts. Additionally, we have also explored the use of these nonwoven Ag/PA66 fabrics for personal thermal management via Joule heating with samples showing rapid heating response (up to 0.2°C/sec) and long-term stability measured over 10,000 seconds. The needle-punched Ag/PA66 nonwoven fabrics, in spite of their low density of the order of 0.04g/cm<sup>2</sup>, exhibited high EMSE values of nearly 69-80dB, leading to excellent weight-normalised specific electromagnetic shielding effectiveness of over 1200 dB/(g/cm<sup>3</sup>) in the 0.015-3GHz range. The production of Ag/PA66 needle punched nonwoven fabrics thus offers a facile route to develop multifunctional fabrics for EMI shielding as well as personal thermal management applications.

**Keywords:** Ag/PA66 fibres; nonwoven; needle punching; electromagnetic shielding; Joule heating; thermal management

## I. Introduction

The advent of wireless technology has seen an exponential increase in the use of electromagnetic wave based devices and architectures such as personal communication equipment, wireless networks among others, resulting in significant electromagnetic interference (EMI) phenomena in both civilian and military applications. To protect not only the sensitive electronic equipment but also humans from the adverse effects of long-term exposure to electromagnetic waves, the continual development of EM shielding materials is essential. Electromagnetic shielding (EMSE) is the process of limiting the penetration of electromagnetic energy into space, by blocking it with barriers made of conductive materials. As compared to traditional metal based EMI shielding materials, polymer composites containing electrically conductive nanofillers (nanotubes, graphene, and metal nanoparticles), conductive metallic yarns and fibres are becoming more attractive owing to their ease of processability, resistance to corrosion and light weight [1]. However, their EM shielding performance is still not comparable to their bulk metal counterparts and thus the rapid development of novel and high performance EMI shielding materials remains an on-going challenge [2-4].

Within the area of EM shielding, a rapid increase in the usage of synthetic fibres coupled with the development of conductive textile materials such as fibres, yarns and fabrics has enabled advances in smart, technical textiles for EM shielding applications [5-8]. Most of the synthetic fibres used in the textiles are electrically insulating materials with the resistivity of the order of  $10^{15} \Omega/\text{cm}^2$ , much higher than the desired resistivity for electromagnetic shielding applications. For example, the resistivity values for anti-electrostatic applications is of the order of  $10^9$  to  $10^{13} \Omega/\text{cm}^2$ , with this value reducing to  $10^2$  to  $10^6 \Omega/\text{cm}^2$  for static dissipation materials. The desired value for electromagnetic shielding materials is lower than  $10^2 \Omega/\text{cm}^2$ . Conductive textile materials have been mainly used for the dissipation of static electricity, transfer of electrical current and signals in wearable electronics and more recently in the production of EM shielding materials. To this effect, silver (Ag) coated polyamide (PA66) fibres are one of the most important conductive textile materials. These commercially available Ag coated polyamide 66 fibres are produced via a chemical bath electroless plating. Electroless plating is a chemical reduction process which depends upon the catalytic reduction of a metallic ion in an aqueous solution containing a reducing agent, and the subsequent deposition of the metal without the use of electrical energy. The metals capable of being deposited by electroless plating include nickel, cobalt, copper, gold, palladium and silver [9,10]. Among all these metals, including copper, Ag offers the highest

1 electrical conductivity ( $6.30 \times 10^7$  S/m), thermal conductivity (398 W/mK) and in conjunction with its  
2 anti-bacterial, anti-fungal, anti-odour and thermal-reflecting properties, makes them an attractive  
3 proposition for the production of multi-functional textile structures [11-17]. However, due to its cost,  
4 silver is generally used in small quantities. For EM shielding applications, electrically conductive textiles  
5 are preferred over metal foils or grids owing to their properties of low weight, elasticity, porosity, air  
6 permeability, low-cost and comfort to the end-user.  
7

8  
9  
10  
11  
12 Now, the technical textiles themselves can be produced through various routes including knitting,  
13 weaving and nonwoven technology. For staple fibres, nonwoven method is the most practical and  
14 preferred method to convert the staple fibres to fabric structures. The nonwoven structures themselves  
15 are largely defined as a random web structure or sheet formed by entangling together the staple fibres  
16 or filament fibres mechanically, thermally or chemically [18-20]. As compared to more conventional  
17 knitting and weaving processes, the nonwoven technique offers significant advantages such as higher  
18 production speed, lower weight material production, ease of use of recycled fibres thereby offering  
19 higher cost-effectiveness. Using suitable fibres and modifications to the technique, a wide variety of  
20 properties can be designed in nonwoven structures such as high breathability, strength, tear-resistance,  
21 absorbance among others which are considered vital for the desired application. The nonwovens  
22 structures have a broad spectrum of end-uses including applications into agriculture, automotive,  
23 medical, hygiene and healthcare among others [21]. Most of the previous literature in the area has been  
24 on the woven and knitted fabrics and composite structures produced from conductive yarns. Only a  
25 handful of reports exist on the use of non-woven technologies for the production of EM shielding fabrics,  
26 which can provide solutions towards low-weight and high shielding efficacy [7,22,23]. In this work, we  
27 demonstrate the use of nonwoven technology to produce high efficiency Ag/PA66 EM shielding fabrics  
28 offering unprecedented shielding efficacy over a wide frequency range. Furthermore, Joule heating  
29 effect is further utilised to make active Ag/PA66 nonwoven fabrics for personal thermal management  
30 applications, thereby providing multifunctional textile structures.  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50

## 51 **II. Experimental Section**

52  
53  
54 **Materials:** The raw material of 3.3 and 6.7dtex Ag-coated PA66 fibres was obtained from R-Stat  
55 Ltd. (France). The 3.3dtex Ag/PA66 fibres have a staple length of 50mm with a diameter of 19-20 $\mu$ m  
56 and were loaded with approximately 20 wt.% Ag. The 6.7dtex Ag/PA66 fibres have a staple length of  
57  
58  
59  
60  
61  
62  
63  
64  
65

60mm with a diameter of 26-27 $\mu$ m with an Ag loading of 12-15 wt.%. The linear electrical conductivity of both the samples is of the order of  $\leq 10^3 \Omega/\text{cm}$ .

**Fabrication of needle punched nonwoven Ag/PA66 fabrics:** The needle punched samples were prepared according to the method described in our previous works [7,22,23]. Briefly, Automatex laboratory type needle punching line, consisting of carding, cross lapper and needle punching machines was used for the production of fabric from staple Ag/PA66 fibres. During the process, the fibres are fed onto the feeding belt of the carding machine (operated at 0.3 m/min) which produces the initial webs. The fibres are carded and combed by worker, stripper, carding drum and comber drum cylinders, respectively. The speeds of these cylinders were kept at 33m/min, 945m/min, 2875m/min and 107m/min, respectively. At the end of the carding machine, parallel laid webs were formed from staple Ag/PA66 fibres. The working speed of carding machine was 15m/min. The webs were oriented to the cross-lapper machine running at approx. 11.50 m/min. The webs were folded at the machine one after the other and transferred to punching machine where the folded webs were needle punched at 250 rpm stroke using the F20 9-22-3/5/5B/Conical 15x17x36x3.5 CBA Foster needles. The feeding and delivery speed of the needle punching machine was 0.8m/min and 1.2m/min. The needle penetration depth was 10mm with a needle punch density of 47.91needle/cm<sup>2</sup>.

### III. Characterisation

#### Physical Characterisation

Differential Scanning Calorimetry (DSC) analysis of the pristine Ag/PA66 fibres was carried out using a DSCQ2000 system (TA Instruments). The fibre samples were carefully rolled using tweezers and then sealed in aluminium crucibles, where they were heated from -50°C to 300°C under 50 ml/min N<sub>2</sub> flow. The melting enthalpy and glass transition temperature were calculated using vendor provided software. To estimate the weight of Ag in Ag/PA66 samples, the pristine staple fibres were subjected to thermogravimetric analysis (TGA) using TA Instruments SDT 2960 DTA-TGA. Samples of approximately 10mg were carefully rolled using tweezers and placed in Pt sample pan. The TGA scans were carried out from 30°C to 700°C at a heating rate of 10°C/min under 100ml/min dry air flow. Fourier transform infra-red spectroscopy (FTIR) analysis was carried out on a Thermo Scientific IS10 Nicolet FTIR spectrometer equipped with the smart TR accessory. Vendor provided OMINIC software was used to analyse the results. The surface morphologies of the Ag/PA66 fibres were observed with a scanning electron microscopy (Hitachi S3400) at an accelerating voltage of 1.5kV. The SEM images of the cross

and longitudinal section of the Ag/PA66 fibres were taken at different magnifications from 1100x to 3000x. The tensile strength test of the Ag/PA66 fibres was carried out using an Instron4411 test device based on the TS EN ISO 5079 standard. The measurements were carried for a 10mm test length at 10mm/min cross-head speed and reported results are an average of ten readings.

### Electromagnetic Shielding Efficiency & Electrical Properties

The EMSE, absorption, reflection and transmission measurements of pre-needled nonwoven fabrics produced was carried out in the frequency range of 0.015-3.0 GHz at room temperature. The fabric samples were cut into circular plates with an areal dimension of 138.85cm<sup>2</sup> to place them between flanges with the measurement area of 37cm<sup>2</sup>. The measurement set-up consists of two coaxial adapters (Electrometrics, EM-2107A), two 10dB attenuators, and a network analyzer (Rohde & Schwarz, ZVL 9 kHz-13GHz). The EMSE calculations were performed using the standard mentioned in ASTM D4935-10 and is described by the following equations:

$$EMSE = 20 \log \left( \frac{E_i}{E_t} \right) \quad (1)$$

where  $E_i$  and  $E_t$  are electrical fields of incident and transmitted radiation, respectively during shielding and no shielding periods. The absorption and reflection values of the sample are calculated using the following Equation 2:

$$A_b = 1 - T_r - R_e \quad (2)$$

where,  $A_b$  and  $R_e$  are the absorbance and reflection of incident radiation, respectively during shielding, and  $T_r$  is transmittance of incident radiation. The values of  $R_e$  and  $T_r$  themselves are calculated using the S parameters according to Equations 3 and 4:

$$R_e = \left| \frac{E_r}{E_i} \right|^2 = |S_{11}(\text{or } S_{22})|^2 \quad (3)$$

$$T_r = \left| \frac{E_t}{E_i} \right|^2 = |S_{21}(\text{or } S_{12})|^2 \quad (4)$$

The surface resistivity measurement of pre-needled nonwoven fabric specimens was carried out in accordance with ASTM D 257-07 standard, using a Keithley6517A electrometer and Keithley8009 resistivity test fixture. Surface resistivity ( $\rho_s$ ) was calculated using the following equation by applying a potential difference across the surface of the specimen and measuring the resultant current:

$$p_s = \frac{53.4V}{I} \Omega \quad (5)$$

where “ $p_s$ ” is the surface resistivity of the needle punched nonwoven fabric specimen, “ $V$ ” is the applied voltage, and “ $I$ ” is the current reading from the instrument [3]. The Joule heating effect in nonwoven fabrics was measured using Farnell PDD3502A Dual 35V, 2A power supply and PICO TC-08 8 channel thermocouple data logger. A sample size of 1” x 1” was connected to the power supply using Cu electrodes pasted (using silver paste) on the fabric sample with the thermocouple mounted on the top surface of the fabric.

**Table 1.** Classification of electromagnetic shielding textiles [48].

## IV. RESULTS and DISCUSSION

### *Physical characterisation of Ag/PA66 fibres*

**Figure 1(a, b)** shows the cross-sectional and longitudinal images of the 3.3 and 6.7dtex (**Fig. 1(d, e)**) Ag/PA66 yarns wherein the presence of the Ag as discrete coating and particles can be clearly observed [9,24]. The fibre diameter for 3.3 and 6.7 dtex fibres was confirmed to be 19 and 26  $\mu\text{m}$ , respectively and is in agreement with the data provided by the manufacturer. The pre needed nonwoven fabrics (PNNF) produced using these fibres are shown in **Fig. 1(c, f)** for 6.7 and 3.3dtex Ag/PA66 fibres. At similar magnifications, as compared to PNNF-6.7 samples, the number density of the fibres for PNNF-3.3 samples is significantly higher. The as-obtained SEM images of nonwoven fabrics were further analysed using the ImageJ image analysis software to measure the fibre density per unit area. The ImageJ software is generally used for viewing fibre orientation distribution, measuring fibre diameter and visualizing 3D images of fibres. As shown in **Fig. 2**, the areas occupied by Ag/PA66 fibres with fineness of 3.3dtex and 6.7dtex in the nonwoven fabrics were found as 72% and 67% respectively [35]. Moreover, the number of fibres per  $\text{cm}^2$  in the PNNF-3.3 and PNNF-6.7 samples were found to be  $\sim 733$  fibres/ $\text{cm}^2$  and 313 fibres/ $\text{cm}^2$  respectively.

**Figure 1.** SEM cross-sectional and longitudinal images of (a, b) 3.3dtex and (d, e) 6.7dtex with the corresponding pre-needed nonwoven fabrics produced from them.

**Figure 2.** Modified threshold map of SEM images of (a) PNNF-3.3 and (b) PNNF-6.7 samples with (c, d) corresponding (ImageJ analysis)

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

**Figure 3(c)** shows the DSC thermograms of the 3.3 and 6.7dtex Ag/PA66 fibres wherein the melting peak of the PA66 can be clearly observed at ~252°C with a melting enthalpy of 63.74J/g and 69.32J/g, respectively. The slightly higher melting enthalpy of 6.7dtex Ag/PA66 fibres translates into enhanced crystallinity for these samples. The corresponding crystallinity,  $\Delta X_c$  (calculated using  $\Delta H_m$  of 100% crystalline PA66 to be 188 J/g) is calculated to be 33.90% and 36.87%, respectively, indicative of the crystallinity of the samples [25]. The small melting peak observed at ~50°C corresponds to the upper glass transition of PA66 due to the reorganisation of crystallites and has been observed by various other authors as well [26,27]. The FTIR spectra of the 3.3dtex and 6.7dtex Ag/PA66 fibres are shown in **Figure 3(b)** and results compared to pristine PA66 pellets. The characteristic vibrations of PA66 are seen at 3297  $\text{cm}^{-1}$  (N-H stretching vibrations from secondary amide groups), 1632  $\text{cm}^{-1}$  (C=O, amide I), 1553  $\text{cm}^{-1}$  (planar N-H deformation, H-N-C=O, amide II) and 1274  $\text{cm}^{-1}$  (amide III stretching vibrations). Additionally, peaks observed at 2931 $\text{cm}^{-1}$  and 2858 $\text{cm}^{-1}$  belonging to CH<sub>2</sub> asymmetric and CH<sub>2</sub> symmetric stretching vibrations, respectively are also observed. The Ag/PA66 shows the characteristic peaks of PA66 however, the intensity of the bands is considerably weakened. Especially, the intensity of peaks at 3297 $\text{cm}^{-1}$  and 1632 $\text{cm}^{-1}$  in the Ag/PA66 fibres are weakened due to interaction of silver and non-bonding electrons in the carbonyl and nitrogen atoms in the amid group of Nylon 66 (H-N-C=O). The silver coated staple polyamide fibres consist of silver particles on polyamide fibres. The deposition of the silver nanoparticles on polyamide fibres caused decreasing of the peak in the Nylon6.6 [31,32]. The loading of Ag on PA66 fibres was measured using TGA analysis as shown in **Fig. 3(a)**. The decomposition of PA66 occurs in the temperature range of 290-550°C with three significant mass losses observed at 320, 435 and 495°C [28,29]. The residual mass left (considered as Ag wt%) was observed to be 18.6 and 12.7% for 3.3 and 6.7dtex Ag/PA66 samples, respectively and is in agreement with the values provided by the manufacturer [30]. In terms of mechanical strength, the 3.3dtex Ag/PA66 fibres displayed a breaking strength of 12.1cN, with the 6.7dtex fibres displaying a much higher value of 25.9cN at similar elongation at break values of nearly 30% (**Fig. 3(d)**). The normalisation of the breaking strength, as a function of dtex value, provided values of 393MPa and 503MPa for 3.3dtex and 6.7dtex Ag/PA66 fibres, respectively.

**Figure 3.** (a) TGA scans showing the residual Ag mass above 600°C, (b) FTIR spectra of 3.3, 6.7dtex Ag-PA66 fibres and its comparison with a pristine PA66 pellets, (c) DSC thermograms (d) stress-strain curves for 3.3dtex and 6.7dtex Ag-PA66 fibres.

## Physical Characterisation of the Ag/PA66 Nonwoven Fabrics

The weight per unit area for the Ag/PA66 nonwoven fabric samples was measured to be 121 and 126 g/m<sup>2</sup>, with the corresponding thickness (measured according to TS EN ISO 9073-2) of 2.64 and 2.87 mm for PNNF-3.3 and PNNF-6.7 samples, respectively. The resulting areal density of the fabrics was thus calculated to be 0.046 and 0.044 g/cm<sup>3</sup> for PNNF-3.3 and PNNF-6.7, respectively. The tensile properties of needle punched nonwoven fabrics were measured on Instron4411 tensile test device according to ASTM D 5034 standard. The breaking strengths of the nonwoven fabrics made from Ag/PA66 fibres with 3.3dtex and 6.7dtex were found 0.20 MPa and 0.28 MPa, respectively. The Young's modulus values of nonwoven fabrics produced from Ag/PA66 fibres with 3.3dtex and 6.7dtex were measured as 0.31 MPa and 0.44 MPa, respectively. In addition to that, it was observed that both the PNNF-3.3 and PNNF-6.7 samples showed high elongation values of up to 127 and 140%, respectively (**Fig. 4**). As these nonwoven fabrics are only pre-needled, these fabrics have low young modulus and breaking strength values. As compared to woven and knitted fabrics, the areal density of nonwoven fabrics is significantly lower and is particularly attractive for wearable applications.

**Figure 4.** Stress-strain curves for nonwoven fabrics made from 3.3 and 6.7 dtex Ag-PA66 fibres

## Electrical and EM shielding properties of Pre-Needled Nonwoven Ag/PA66 Fabrics

Surface resistivity is electrical resistance over a unit area of materials surface and is the resistance to the leakage of current along the materials surface [33,34]. Now, for EM shielding materials, the surface resistivity values are of prime importance with low resistivity (i.e. high electrical conductivity) favouring the enhancement of EM shielding effect [4]. The surface resistivity of pre-needled nonwoven fabrics produced from silver coated staple polyamide fibres with fineness of 6.7dtex and 3.3dtex are measured to be 2.75E+02Ω and 1.17E+02Ω. The results clearly show that while both the pre-needled nonwoven fabrics are highly conductive; the PNNF-3.3 nonwoven fabric shows much lower surface resistivity. This increase in the conductivity values can be attributed to the higher loading of Ag (18.6 wt%) for 3.3dtex Ag/PA66 fibres as compared to the 12.7wt% for 6.7dtex Ag/PA66 fibres.



1 **Figure 5.** (a) EMSE response and (b) absorption and reflection results of PNNF-3.3 and PNNF-6.7  
2 samples in the 0.15-3.0GHz range, (c) comparison of specific EMSE values of our samples with other  
3  
4 reported results of nonwoven fabrics obtained from [7, 22, 23]  
5  
6

7 The EMSE response of PNNF-3.3 and PNNF-6.7 nonwoven fabrics measured between 0.015-  
8 3GHz frequency range are presented in **Fig. 5(a)**. It can be clearly observed that the EM shielding  
9 properties of both the nonwoven fabrics are remarkably high in spite of their low weight per square  
10 meters of 120-126g/m<sup>2</sup>. Moreover, as compared to PNNF-6.7, the PNNF-3.3 samples consistently  
11 showed 4-5dB higher EMSE values across the whole of the frequency range. This difference became  
12 more significant at higher frequency values, especially above 2.1GHz where the difference reached  
13 nearly 13dB at 2.4GHz. This increase in the EMSE values for PNNF-3.3 samples throughout the  
14 frequency range can be explained by considering the fact that the as the fineness of fibre reduces from  
15 6.7dtex to 3.3dtex, the number of conductive Ag/PA66 fibres in the nonwoven structure increases, which  
16 enhances the conductivity and consequently the EMSE. This increase in the number of Ag/PA66 fibres  
17 for PNNF-3.3 samples can be observed in the SEM image of the fabrics in **Fig. 2**. **Figure 5(b)** shows  
18 the reflection and absorption behaviour of the nonwoven Ag/PA66 fabrics. It can be clearly observed  
19 that the absorption values of both the PNNF-3.3 and PNNF-6.7 samples are gradually increasing with  
20 a difference of 3-4dB in their respective absorption values, with higher absorption values observed in  
21 the high frequency range (1.5-3GHz). Consequently, the reflection values observed across the  
22 measurement range showed an opposite trend to the absorption values, with the reflection values  
23 decreasing with an increase in the frequency. It was observed that as fibre fineness reduces from  
24 3.3dtex to 6.7dtex, in the other words, as the fibre is coarse, the absorption values of pre-needled  
25 nonwoven fabric produced from this kind of the fibres increase too. Similarly, the reflection values for  
26 PNNF-3.3 samples are consistently higher than the PNNF-6.7 samples. As mentioned earlier as well,  
27 with an increase in the fibre fineness, the number of fibres increase (per unit area) for 3.3dtex Ag/PA66  
28 samples. Therefore, it is believed that the values of reflection for PNNF-3.3 are higher due to this  
29 increase in the number of fibres per unit area. It should be mentioned that the transmission values for  
30 both the pre-needled nonwoven fabrics are close to zero due to the high reflection and absorption  
31 values observed. According to Equation2, it can be seen that the reflection and absorption become  
32 large, while transmission reduces.  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

1 It was observed that both of pre-needled nonwoven fabrics have shielding effectiveness of more  
2 than 30dB (99.9% or better) in the 0.3-3.0GHz frequency range. An EMSE value of 30dB or more is  
3 classified as “excellent” and graded with “AAAAA” in Class II-General Use by the Committee for  
4 Conformity Assessment on Accreditation and Certification of Functional and Technical Textiles. The  
5 highest EMSE value of 82.1 dB was observed for the sample PNNF-3.3 at a frequency of 2.4GHz, with  
6 the samples showing an increase in the EMSE from 23.1dB (for 0.15GHz) to 77.3dB (at 3.0GHz). The  
7 PNNF-6.7 samples in the same range showed the highest EMSE value of 68.8 dB, with an increase in  
8 the EMSE from 19.2dB (for 0.15GHz) to 64.9dB (for 3.0GHz). These shielding characteristics thus  
9 classify the samples as “excellent” for general use. For professional use, these pre-needled nonwoven  
10 fabrics reach 99.9999% shielding effectiveness after 1.8GHz and can thus be classified as “excellent”  
11 for high frequency range for professional use. The specific EM shielding efficiency was calculated on  
12 the basis of the rate of total EMI shielding efficiency and the fabric density, and the results are shown  
13 in Figure 4(c). The specific EM shielding efficiency of the PNNF-6.7 and PNNF-3.3 was calculated to  
14 be 1217 dB/(g/cm<sup>3</sup>) and 1270 dB/(g/cm<sup>3</sup>), respectively. Owing to the greater density of fibres per unit  
15 area, the specific EM shielding efficiency representing the material utilisation efficiency, is slightly higher  
16 than the PNNF-6.7 fabrics, again demonstrating the effect of fineness of the Ag/PA66 fibres on the EM  
17 shielding effect. Figure 5(c) provides a comparison of the values obtained from the literature for other  
18 reported nonwoven fabrics using polyester (PES) and stainless steel (SS) fibres. Due to the much  
19 higher density of the PES-SS samples, the weight normalised EMSE values of pre-needled nonwoven  
20 fabrics produced from Ag/PA66 fibres are approximately 5 times higher than the nonwoven fabrics  
21 made from 50% PES-SS [36]. Chen et al have reported on the production of co-weaving-knitting fabric  
22 reinforced composites using stainless steel/copper/polyamide yarns exhibiting high EM shielding values  
23 of nearly 40-50 dB. However, due to the extensive use of stainless steel, the density of the samples  
24 was very high at 1.47 g/cm<sup>3</sup> leading to a density specific EMSE of 34.02 dB/(g/cm<sup>3</sup>). The EM shielding  
25 properties of nanofiber based nonwoven materials coated with Ni-Fe metallic films via sputtering.  
26 Electrospinning was used to produce nanofibers of ~500 nm diameter followed by Ni-Fe coating of 100-  
27 400 nm thickness resulting in attenuation of nearly 99.98% of electromagnetic waves in the 6-13 GHz  
28 region [38]. Similarly, Avloni et al have investigated the EM shielding behaviour of Polypyrrrole coated  
29 nonwoven fabrics where a maximum attenuation of 37dB was obtained. Koprowska et al have used a  
30 polyurethane/ polyacrylonitrile layer containing electro conductive fillers such as carbon nanotubes and  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

1 nanofibers in conjunction with a needle-punched polyester nonwoven fabric. The composite exhibited  
2 a shielding efficiency of 6-20 dB only, which is significantly lower than our samples. The needle punched  
3 nonwoven fabrics made from Ag/PA66 fibres have continuously increasing EMSE behaviour between  
4 0.15-3GHz frequency range, while the woven stainless steel-polyester fabrics show continuously  
5 decreasing EMSE behaviour at the same frequency range. The highest EMSE value obtained was 41dB  
6 at a rather low frequency of 360MHz with woven fabric made of acrylic based hybrid yarns containing  
7 metal stainless steel wire, while the highest EMSE value was found 82.1dB at 2.4GHz high frequency  
8 with needle punched nonwoven fabric made from Ag/Pa66 fibres with fineness of 3.3dtex. As the  
9 frequency increases in the 0.5-3GHz frequency range, the EMSE values of the woven fabrics with metal  
10 wire tends to decrease, while the EMSE values of the needle punched nonwoven fabrics with  
11 conductive silver coated polyamide fibre tend to increase [37]. In another study, the shielding  
12 effectiveness of silver plated polyacrylonitrile (PAN) fabric in the 30kHz and 3GHz frequency range was  
13 investigated and found as 40-80dB. After washing for over 30 times, the shielding value decreased to  
14 35-50dB [38]. We envisage that due to their low weight and excellent EM shielding characteristics,  
15 these nonwoven fabrics can be used for technical textile applications such as interlining fabric for  
16 wearable garment, military tent and shielding fabric for building [48].  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31

32  
33  
34 **Figure 6.** (a) Temperature evolution for PNNF -6.7 fabric samples as a function of applied voltage, (b)  
35 stability of temperature response measured over 10,000 seconds.  
36  
37  
38  
39

40 Temperature control is one of the most basic functions of textiles and for active clothing and there  
41 is a strong demand to produce active structures which are not only lightweight but also provide control  
42 over the heating. Passive clothing is not suitable in applications where the end-user undertakes a large  
43 amount of work as the large number of layers hinder the movement [44]. Most of the heating elements  
44 use the Joule's heating principle in which heat is generated as electric current flows through the  
45 conductive material. Conductive materials such as metals, metal coated fibres and conducting polymers  
46 have been used in many textile applications for making heating elements. These active textile based  
47 heating elements have been manufactured using various textile production techniques such as knitting,  
48 weaving and nonwoven technology [43-45]. However, it has been shown in the literature that heating  
49 elements made from nonwoven structures suffer from high electrical resistance, thereby limiting their  
50 use as compared to knitted and woven structures with the woven fabric showing lower resistance as  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

1 compared to knitted structures [46]. As observed in **Fig. 6(a)**, the PNNF-6.7 sample shows a rapid  
2 increase in the temperature as a function of applied potential which can be attributed to the rather low  
3 mass density of the samples. The temperature was measured using a thermocouple in close contact  
4 with the 1" x 1" specimen. As the Joule heating is inversely proportional to the resistivity, the PNNF-3.3  
5 samples showed a slightly lower peak temperature than the PNNF-6.7 samples (**Fig. 6(b)**) at the same  
6 applied voltages during the stability test carried out for 10,000 seconds. The PNNF-6.7 sample showed  
7 an average stable temperature reading of  $33.52 \pm 0.47$  °C whereas the PNNF-3.3 sample showed an  
8 average stable temperature of  $32.38 \pm 0.48$  °C over the measurement. These values are comparable  
9 to those obtained by Ag nanowire coated textiles and knitted, woven fabrics obtained using Ag coated  
10 yarns [47].  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20

## 21 CONCLUSIONS

22  
23  
24 In this work, the electromagnetic shielding effectiveness of nonwoven fabrics produced from  
25 conductive Ag/PA66 staple fibres with fineness of 6.7dtex and 3.3dtex was investigated. The fabrics  
26 samples were further characterised using surface resistivity analysis as well as electron microscopy  
27 and infrared spectroscopy analysis. The needle-punched Ag/PA66 nonwoven fabrics, in spite of their  
28 low density of the order of  $0.04\text{g/cm}^2$ , exhibited high EMSE values of nearly 69-80dB, leading to  
29 excellent weight-normalised specific electromagnetic shielding effectiveness of over  $1200\text{ dB}/(\text{g/cm}^3)$  in  
30 the 0.015-3GHz range. The nonwoven fabric produced using 3.3dtex Ag/PA66 fibres, PNNF-3.3,  
31 showed higher EMSE values as compared to the 6.7dtex nonwoven fabrics due to higher fibre density  
32 and lower resistivity. Further analysis of the EM shielding behaviour led to the conclusion that the  
33 reflection (absorption) values for PNNF-3.3 samples was higher (lower) than PNNF-6.7 samples across  
34 the 0.015-3.0GHz range. Concurrently, the transmission values measured were negligible across the  
35 whole range, suggesting that these fabrics are highly suitable for most of the class-II (general) uses and  
36 many class-I (professional) applications such as protective wearable textiles and building textiles. Due  
37 to their high conductivity, the samples were further utilised as Joule heating fabrics for application into  
38 personal thermal management. Both the PNNF-3.3 and PNNF-6.7 nonwoven samples showed voltage  
39 dependent, rapid heating rates with the PNNF-6.7 samples showing a better and stable response due  
40 to the higher thickness of the fabric. Thus, the production of Ag/PA66 needle punched nonwoven fabrics  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

1 offers a facile route to develop multifunctional fabrics for EMI shielding as well as personal thermal  
2 management applications.  
3

## 4 **ACKNOWLEDGEMENTS**

5 The authors would like to thank R-Stat Ltd. (France) for providing Ag/PA66 staple fibres,  
6  
7 TUBITAK (The Scientific and Technological Research Council of TURKEY) for providing the financial  
8 support to Dr. Mustafa Sabri Ozen and University of Bolton. The first author was supported by TUBITAK  
9 (The Scientific and Technological Research Council of TURKEY) in the framework 2219 International  
10 Post-Doctoral Research Fellowship Programme. This work was supported by the Scientific Research  
11 Project Unit (BAPKO) of the Marmara University (project number FEN-A-110913-0375).  
12  
13  
14  
15  
16  
17  
18  
19  
20

## 21 **REFERENCES**

- 22 1. B. Shen, W. Zhai, M. Tao, J. Ling, W. Zheng, "Lightweight, Multifunctional Polyetherimide/  
23 Graphene@Fe<sub>3</sub>O<sub>4</sub> Composite Foams for Shielding of Electromagnetic Pollution", Appl. Mater. &  
24 Interfaces, 5, pp. 11383-11391 (2013).  
25
- 26 2. W.L. Song, M.S. Cao, M.M. Lu, B. Song, C.Y. Wang, J. Liu, J. Yuan, L.Z. Fan "Flexible  
27 Graphene/Polymer Composite Films in Sandwich Structures for Effective Electromagnetic  
28 Interference Shielding", Carbon, 66, pp. 67-76 (2014).  
29
- 30 3. F.Z. Engin, I. Usta, "Electromagnetic Shielding Effectiveness of Polyester Fabrics with Polyaniline  
31 Deposition", Textile Research J., 84, 9, pp. 903-912 (2014).  
32
- 33 4. Z. Yildiz, I. Usta, A. Gungor, "Electrical Properties and Electromagnetic Shielding Effectiveness of  
34 Polyester Yarns with Polypyrrole Deposition", Textile Research J., 82, 20, pp. 2137-2148 (2012).  
35
- 36 5. A.K Rakshit, M.A. Hira, "Electrically Conductive Fibre Substrates", International J. of Fiber and  
37 Textile Research, 4, 3, pp. 44-48 (2014).  
38
- 39 6. K. Jagatheesan, A. Ramasamy, A. Das, A. Basu, "Electromagnetic Shielding Behaviour of  
40 Conductive Filler Composites and Conductive Fabrics-A Review", Indian Journal of Fibre & Textile  
41 Research, 39, pp. 329-342 (2014).  
42
- 43 7. M.S. Ozen, E. Sancak, A. Beyit, I. Usta, M. Akalin, "Investigation of Electromagnetic Shielding  
44 Properties of Needle-Punched Nonwoven Fabrics with Stainless Steel and Polyester Fiber", Textile  
45 Research J., 83, 8, pp. 849-858 (2013).  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65

- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65
8. H. Aniolczyk, J. Koprowska, P. Mamrot, J. Lichawska, "Application of Electrically Conductive Textiles as Electromagnetic Shields in Physiotherapy", *Fibres & Textiles in Eastern Europe*, 12, 4, 48, pp. 47-50 (2004).
9. R. Perumalraj, B.S. Dasaradan, "Electroless Nickel Plated Composite Textile Materials for Electromagnet Compatibility", *Indian J. of Fibre & Textile Research*, 36, pp. 35-41 (2011).
10. C. Xu, R. Zhou, H. Chen, "Silver-Coated Glass Fibres Prepared By a Simple Electroless Plating Technique", *J. of Materials Science-Materials in Electronics*, 25, 10, pp. 4638-4642 (2014).
11. K.K Goli, N. Gera, X.M. Liu, B.M. Rao, O.J. Rojas, J. Genzer, "Generation and Properties of Antibacterial Coatings Based on Electrostatic Attachment of Silver Nanoparticles to Protein-Coated Polypropylene Fibres", *ACS Appl. Mater. & Interfaces*, 5, 11, pp. 5298-5306 (2013).
12. M. Zieger, C. Wiegand, A. Krahmer, "Antibacterial and Antifungal Properties of a Silver-Coated Fiber", *Experimental Dermatology*, 22, 3, pp. 46 (2013).
13. F.B. Yu, Y. Chen, "Preparation of Antibacterial Silver Plated Fiber and Its Performance", *Electroplating & Finishing*, 31, 11, pp. 36-8 (2013).
14. M. Raymer, "The Silicon Web-Physics for the Internet Age", Taylor & Francis, pp. 153 (2009).
15. P. Cognard, "Adhesives and Sealants, Basic Concepts and High Tech Bonding, Handbook of Adhesives and Sealants", Elsevier Ltd, pp. 382 (2005).
16. P. Warriar, A. Teja, "Effect of Particle Size on The Thermal Conductivity of Nanofluids Containing Metallic Nanoparticles", *Nanoscale Research Lett*, 6, 247, pp. 1-6 (2011).
17. J. Matricon, G. Waysand, C. Glashausser, "The Cold Wars: A History of Super Conductivity", Rutgers University Press, ISBN-0-8135-3295-7, pp. 32 (2003).
18. I.M Hutten, "Handbook of Nonwoven Filter Media", Butterworth-Heinemann, UK, ISBN-10: 1-8561-7441-7, pp. 2-4 (2007).
19. W. Zhong, "An Introduction to Healthcare and Medical Textiles", DEStech Publications, USA, ISBN: 978-1-60595-020-4, pp. 31 (2013).
20. D. Das, B. Pourdeyhimi, "Composite Nonwoven Materials Structure, Properties and Applications", Woodhead Publishing Series in Textiles, ISBN: 978-0-85709-770-5, pp. 3-4 (2014).
21. W. Albrecht, H. Fuchs, W. Kittelmann, "Nonwoven Fabrics: Raw Materials, Manufacture, Applications, Characteristics, Testing Processes", WILEY-VCH GmbH&Co.KGaA, Weinheim, Federal Republic of Germany, ISBN:3-527-30406-1 (2003).

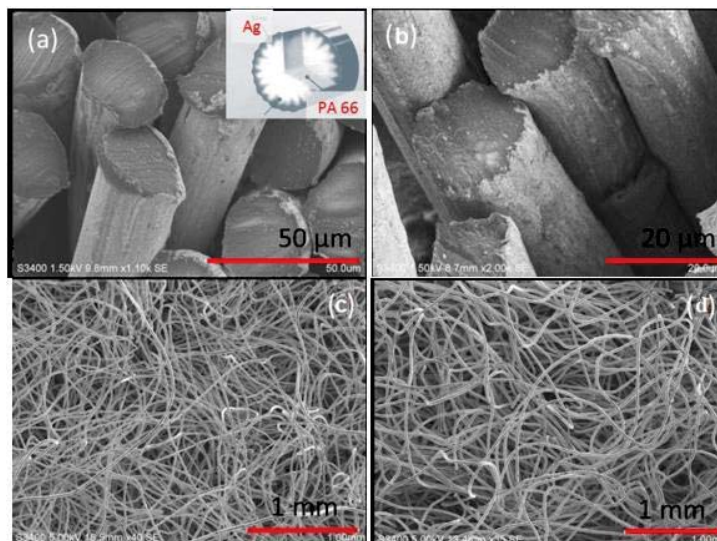
- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65
22. M.S. Ozen, "Investigation of the Electromagnetic Shielding Effectiveness of Carded and Needle Bonded Nonwoven Fabrics Produced at Different Ratios with Conductive Steel Fibers", *J. of Fiber and Fabrics*, 10, 1, pp. 140-151 (2015).
  23. M.S. Ozen, E. Sancak, M. Akalin, "The Effect of Needle-Punched Nonwoven Fabric Thickness on Electromagnetic Shielding Effectiveness", *Textile Research J.*, DOI: 10.1177/0040517514555794, 85, 8, pp. 804-815 (2015).
  24. D. Hegemann, M. Amberg, A. Ritter, M. Heuberger, "Recent Developments in Ag Metallised Textiles Using Plasma Sputtering", *Mater. Technology*, 24, 1, pp. 41-45 (2009).
  25. H.W. Starkweather, P. Zoller, G.A. Jones, "The heat of fusion of 66 nylon", *J. of Polym. Sci.*, 22, 9, pp. 1615-1621 (1984).
  26. M. Duhovic, P. Maitrot, S. Fakirov, "Polyamide66 Polymorphic Single Polymer Composites", *The Open Macromolecules J.*, 3, pp. 37-40 (2009).
  27. X. Zhang, Y.B. Li, Y. Zuo, G.Y Lu, Y.H. Mu, H. Li, "Morphology, Hydrogen-Bonding and Crystallinity of Nano-Hydroxyapatite66 Bio composites", *Composites Part A*, 38, pp. 843-848 (2008).
  28. S. Pashaei, A. Souldozi, S.U.T. Syed, A.A Syed, "Investigation on Thermal and Mechanical Behaviours of Crysnanoclay Incorporated Polyamide/Nanoclay Composites", *International J. of Chemtech Research*, 3, 3, pp. 1292-1301 (2011).
  29. M. Herrera, G. Matuschek, A. Kettrup, "Main Products and Kinetics of the Thermal Degradation of Polyamides", *Chemosphere*, 42, pp. 601-607 (2001).
  30. K. Varga, M.F. Noisterning, U.J. Griesser, L. Alja, T. Koch, "Thermal and Sorption Study of Flame Resistant Fibers", *Lenzinger Berichte*, 89, pp. 50-59 (2011).
  31. N. Perkasi, G. Amirian, S. Dubinsky, S. Gazit, A. Gedanken, "Ultrasound-Assisted Coating of Nylon6.6 with Silver Nanoparticles and Its Antibacterial Activity", *J. of Appl. Poly. Sci.*, 104, pp. 1423-1430 (2007).
  32. P.F. Navarro, B.G. Martinez, H.A.L. Martinez, V.M. Castano, A.J.S. Rivera, R.F. Medellin, S. C. Velasco, "Effects on the Thermo-Mechanical and Crystallinity Properties of Nylon6.6 Electrospun Fibres Reinforced with One Dimensional (1D) and Two Dimensional (2D) Carbon", *Materials*, 6, pp. 3494-3513 (2013).
  33. L. Rupprecht, "Conductive Polymers and Plastics in Industrial Applications", *Society of Plastics Engineers, Plastics Design Library*, ISBN 1-884207-77-4, Canada, pp.145 (1999).



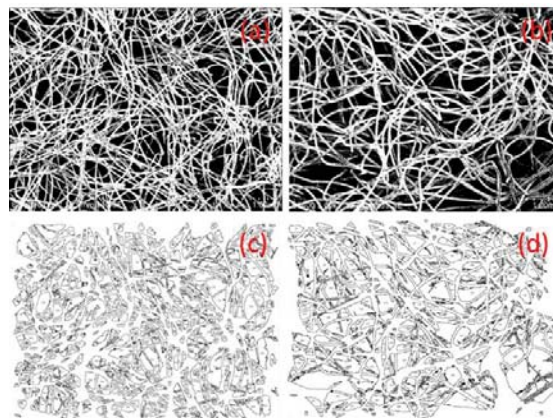
- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65
34. V.R. Sastri, "Plastics in Medical Devices: Properties, Requirements, and Applications: Polymer Additives Used to Enhance Material Properties for Medical Device Applications", Elsevier Inc., United States of America, ISBN: 978-1-4557-3201-2, pp. 63 (2014).
  35. C.G. Chinga, M. Lenes, P.O. Johnsen, E.L. Hult, "Computer-Assisted Scanning Electron Microscopy of Wood Pulp Fibres: Dimensions and Spatial Distributions in a Polypropylene Composite", *Micron*, 40, pp. 761-768 (2009).
  36. J. Ling, W. Zhai, W. Feng, B. Shen, J. Zhang, W. Zheng, "Facile Preparation of Lightweight Microcellular Polyetherimide/Graphene Composite Foams for Electromagnetic Interference Shielding", *Appl. Mater. & Interfaces*, 5, pp. 2677-2684 (2013).
  37. H.C. Chen, K.C. Lee, J.H. Lin, "Electromagnetic and Electrostatic Shielding Properties of Co-Weaving-Knitting Fabrics Reinforced Composites", *Composites Part A: Appl. Sci. and Manufacturing*, 35, pp. 1249-1256 (2004).
  38. M. Sonehara, T. Sato, M. Takasaki, H. Konishi, Y. Miura, M. Yamaguchi, "Preparation and Characterization of Nano-Fiber Nonwoven Textile for Electromagnetic Wave Shielding," *IEEE Transactions on Magnetics*, 44, 11, pp. 3107-3110 (2008).
  39. J. Avloni, R. Lau, M. Ouyang, L. Florio, A.R. Henn, A. Sparagniva, "Polypyrrole Coated Nonwovens for Electromagnetic Shielding", *J. of Industrial Textiles*, 38, 1, pp. 55-68 (2008).
  40. J. Koprowska, M. Leonowicz, "Electro conductive Polymer Matrix Nanocomposites Exhibit Shielding Properties", *EMC Europe International Symposium on Electromagnetic Compatibility* (2009).
  41. A. Bedeloglu, "Investigation of Electrical, Electromagnetic Shielding, and Usage Properties of Woven Fabrics Made from Different Hybrid Yarns Containing Stainless Steel Wires", *J. of the Textile Institute*, 104, 12, pp. 1359-1373 (2013).
  42. W. Wang, W. Li, C. Gao, W. Tian, B. Sun, D. Yu, "A Novel Preparation of Silver-Plated Polyacrylonitrile Fibers Functionalized with Antibacterial and Electromagnetic Shielding Properties", *Appl. Surface Sci.*, 342, pp.120-126 (2015).
  43. M. Neruda, L. Vojtech, "Heating Ability of Electrically Conductive Textile Materials", *Proceedings of the 16<sup>th</sup> International Conference on Mechatronics, Mechatronika, Czech Republic*, pp. 631-634 (2014).



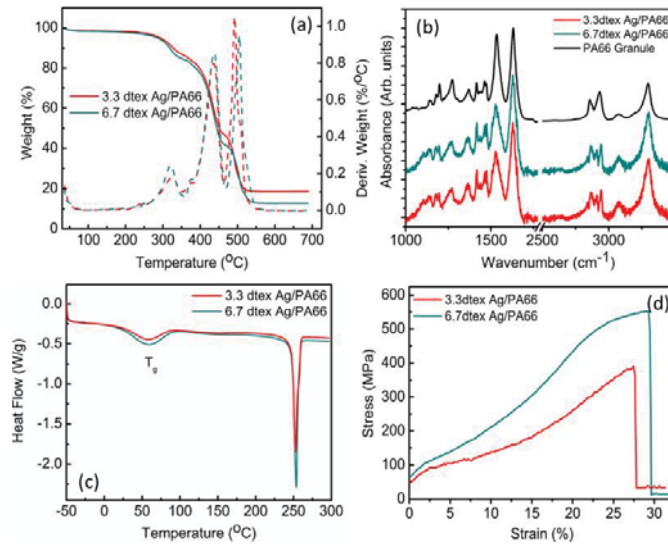
- 1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57  
58  
59  
60  
61  
62  
63  
64  
65
44. M.S. Poboroniuc, A. Curteza, V. Cretu, L. Macovei, "Designing Wearable Textile Structures with Embedded Conductive Yarns and Testing Their Heating Properties", International Conference and Exposition on Electrical and Power Engineering, Romania, pp.778-783 (2014).
  45. L. Hao, Z. Yi, C. Li, X. Li, W. Yuxiu, G. Yan, "Development and Characterization of Flexible Heating Fabric Based on Conductive Filaments", Measurement, 45, 7, pp. 1855-1865 (2012).
  46. S. Hamdani, P. Potluri, A. Fernando, "Thermo-Mechanical Behavior of Textile Heating Fabric Based on Silver Coated Polymeric Yarn", Materials, 6, 3, pp. 1072-1089 (2013).
  47. P.C. Hsu, X. Liu, C. Liu, X. Xie, H.R. Lee, A.J. Welch, T. Zhao, Y. Cui, "Personal Thermal Management by Metallic Nanowire-Coated Textiles", Nano Lett., 15, 1, pp. 365-371 (2015).
  48. FTTS-FA-003 Test method of specified requirements of electromagnetic shielding textiles, Committee for Conformity Assessment on Accreditation and Certification of Functional and Technical Textiles: Taiwan. pp. 1-4 (2005).



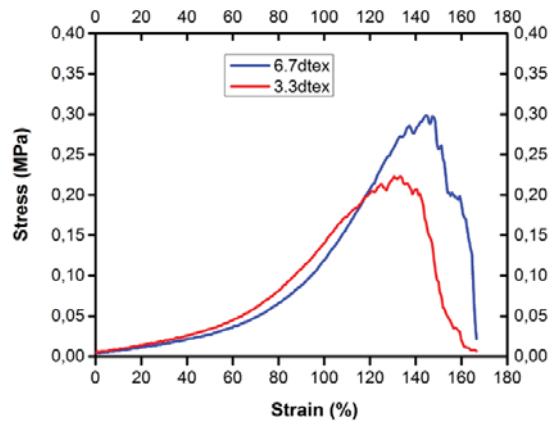
**Figure 1.** The cross-sectional (SEM) images of 3.3dtex (a) and 6.7dtex (b) silver coated PA66 fibres. The longitudinal (SEM) images of corresponding pre-needled nonwoven fabrics produced from 3.3dtex (c) and 6.7dtex (d) silver coated PA66 fibres.



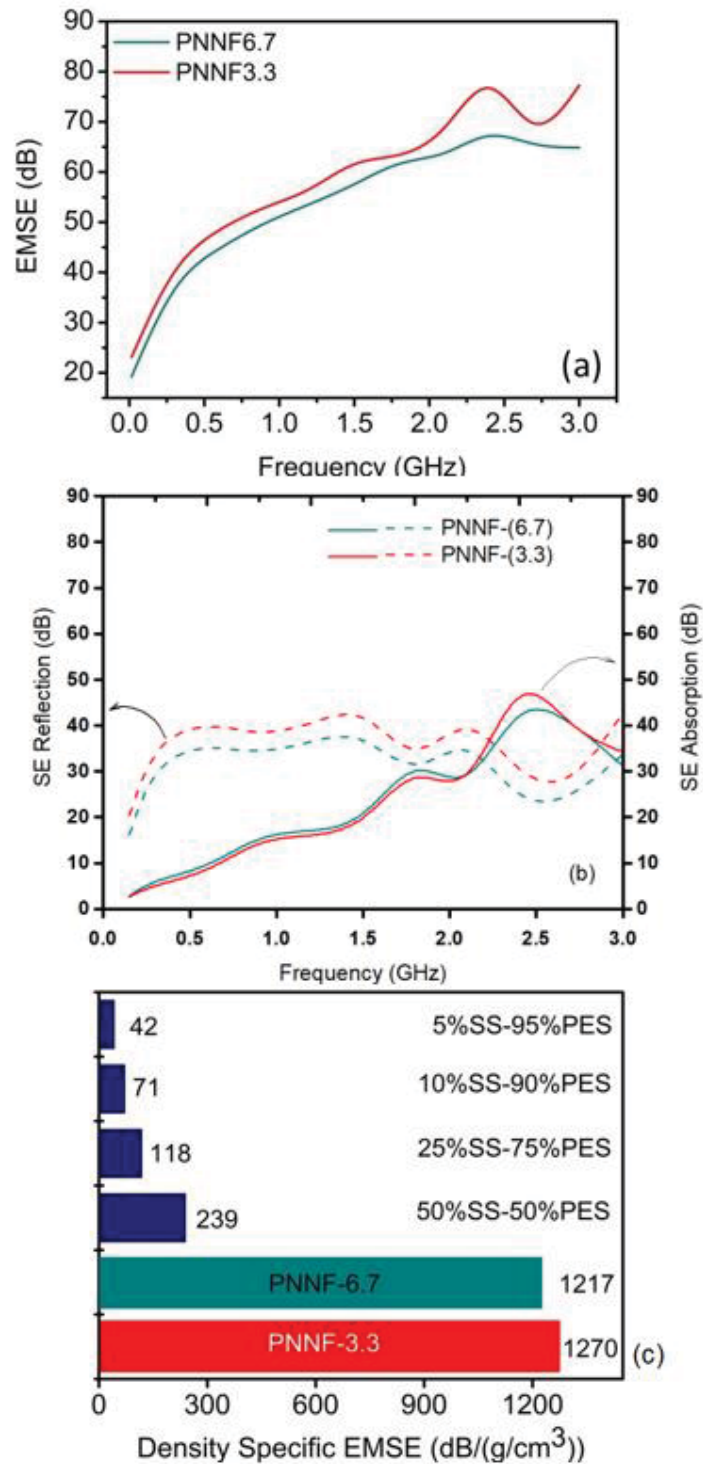
**Figure 2.** Modified threshold map of SEM images of (a) PNNF-3.3 and (b) PNNF-6.7 samples with (c, d) corresponding (ImageJ analysis)



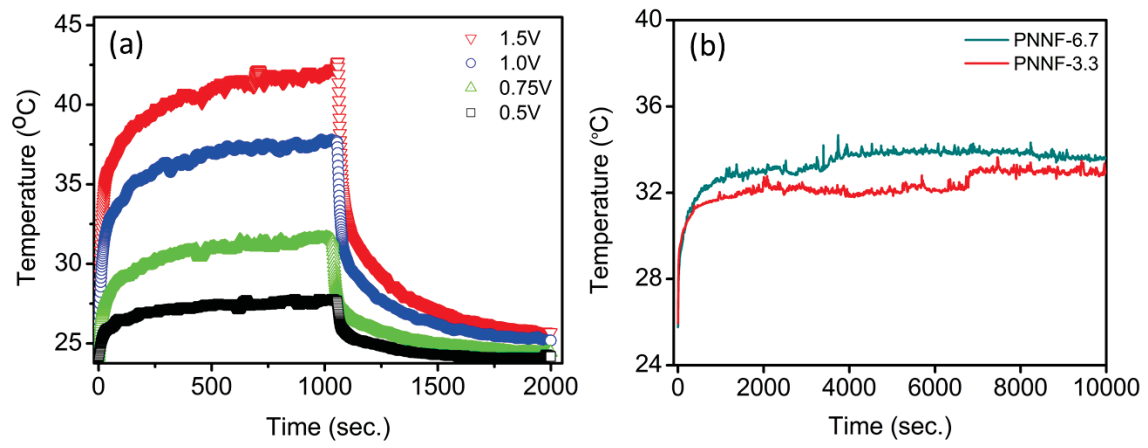
**Figure 3.** (a) TGA scans showing the residual Ag mass above 600°C, (b) FTIR spectra of 3.3, 6.7dtex Ag-PA66 fibres and its comparison with a pristine PA66 pellets, (c) DSC thermograms (d) stress-strain curves for 3.3dtex and 6.7dtex Ag-PA66 fibres.



**Figure 4.** Stress-strain curves for nonwoven fabrics made from 3.3 and 6.7 dtex Ag-PA66 fibres



**Figure 5.** (a) EMSE response and (b) absorption and reflection results of PNNF-3.3 and PNNF-6.7 samples in the 0.15-3.0GHz range, (c) comparison of specific EMSE values of our samples with other reported results of nonwoven fabrics obtained from Ref. [7,22,23]



**Figure 6.** (a) Temperature evolution for PNNF -6.7 fabric samples as a function of applied voltage, (b) stability of temperature response measured over 10,000 seconds.

**Table 1.** Classification of electromagnetic shielding textiles [48].

Type	Grade	Shielding effectiveness (dB)	Classification	Electromagnetic Shielding, ES (in %)
Class I Professional use	AAAAA	$SE > 60\text{dB}$	Excellent	$ES > 99.9999\%$
	AAAA	$60\text{dB} \geq SE > 50\text{dB}$	Very good	$99.9999\% \geq ES > 99.999\%$
	AAA	$50\text{dB} \geq SE > 40\text{dB}$	Good	$99.999\% \geq ES > 99.99\%$
	AA	$40\text{dB} \geq SE > 30\text{dB}$	Moderate	$99.99\% \geq ES > 99.9\%$
	A	$30\text{dB} \geq SE > 20\text{dB}$	Fair	$99.9\% \geq ES > 99.0\%$
Class II General use	AAAAA	$SE > 30\text{dB}$	Excellent	$ES > 99.9\%$
	AAAA	$30\text{dB} \geq SE > 20\text{dB}$	Very good	$99.9\% \geq ES > 99.0\%$
	AAA	$20\text{dB} \geq SE > 10\text{dB}$	Good	$99.0\% \geq ES > 90\%$
	AA	$10\text{dB} \geq SE > 7\text{dB}$	Moderate	$90\% \geq ES > 80\%$
	A	$7\text{dB} \geq SE > 5\text{dB}$	Fair	$80\% \geq ES > 70\%$