

1 Reliability of ground reaction forces in the aquatic environment

2

3 1. Introduction

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5 **Bipedal gait is a skilled and complex activity** that requires coordinated
6 and controlled movements of the limbs, which act alternately from one support
7 position to another. Gait can be studied and evaluated in various ways, one of
8 which is through the use of force plates (FPs) that measure the direction and
9 magnitude of the ground reaction forces (GRFs) (Duarte and Freitas, 2010).
10 GRFs are of equal magnitude and the opposite direction to the force the body
11 exerts on the ground through the foot, and must be overcome during forward
12 movement (Sutherland, 2005).

13 Aquatic exercises are widely used in the treatment of patients with many
14 different medical conditions; these exercises maximize the properties of water
15 related to fluid mechanics, such as viscosity, drag force, turbulent flow and
16 buoyancy to achieve best outcomes for patients. Water is an ideal environment
17 for exercise due to the decreased weight bearing through the lower limbs,
18 offering less impact throughout the stance phase of the gait, but exercise in
19 water also requires greater propulsive force to overcome the force of water
20 (Harrison and Bulstrode, 1987; Nakazawa *et al.*, 1994 and Barela *et al.*,
21 2006). The magnitude of the gait GRFs although lower than on land, can still be
22 excessive, depending on the individual patient and their condition or medical
23 problem. Knowing the GRFs related to different underwater activities during
24 rehabilitation would help in exercise prescription and the evaluation of patients
25 in this environment (Haupenthal *et al.*, 2010c).

26 In 1992, Harrison *et al.* investigated GRFs in the aquatic environment.
27 The authors designed a waterproof FP using a silicon rubber compound to
28 measure weight-bearing during underwater gait at two heights of water
29 submersion (1.1 and 1.3 m) and patients walked at two different speeds (slow
30 and fast). The authors found that the percentage of weight bearing decreases
31 inversely proportional to the speed. Since this seminal work, several other
32 studies have explored GRFs in water during different activities such as running,
33 jumping, backward walking and stationary running, factors such as depth of
34 immersion and gait velocity have also been considered (Haupenthal *et al.*,
35 2010a; Haupenthal *et al.*, 2010b; Orselli and Duarte, 2011; Fontana *et al.*, 2011;
36 Donoghue *et al.*, 2011; Carneiro *et al.*, 2012; Fontana *et al.*, 2012 and
37 Haupenthal *et al.*, 2013).

38 The use of reliable methods to determine the outcome of clinical
39 interventions is essential as outcomes (or lack of outcomes) can have serious
40 implications for patients. Visual and observational assessment methods are
41 subjective and may not accurately reflect the results of treatment intervention.
42 Thus, reliability studies are needed to evaluate the error in any outcome
43 measure and test-retest studies are required to determine how well any
44 measure performs at different times (Rankin and Stokes, 1998). Such studies
45 may provide data about consistency as well demonstrating the safe use of the
46 outcome measure not only in clinical practice but also in biomechanics research
47 (Portney and Watkins, 2000 and Lexell and Downham, 2005).

48 Several studies have evaluated the reliability of the FP during gait on
49 land in different conditions and with different populations (Kadaba *et al.*, 1989;
50 Hamill and McNiven, 1990; White *et al.*, 1999; Fortin *et al.*, 2008 and Veilleux *et*

51 *al.*, 2012). However, to date there are no studies assessing the reliability of the
52 FP in underwater walking. This is a major gap in the literature considering the
53 extent to which aquatic exercises are used in rehabilitation and the need for a
54 reliable outcome measure. The immersed body is affected by the action of fluid
55 mechanics, which of course influences gait, thus establishing the reliability of
56 kinetic parameters of underwater gait is necessary. The aim of this study
57 therefore was to investigate the test-retest reliability of the kinetic gait
58 parameters, as measured by a FP, in healthy individuals in water.

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60 **2. Method**

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62 *2.1 Participants*

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64 Forty-nine healthy young volunteers participated in this study, 31 females
65 and 18 males, with a median (Md (25-75%)) age of 21 years (20-22), mass of
66 57.5 kg (53-68), weight in the water of 147 N (98-225.5) and height of 1.65 m
67 (1.60-1.72). The volunteers were considered eligible if they were between 18
68 and 24 years and had no current lower extremity musculoskeletal pain and/or
69 injury or any disorder affecting sensation in the lower extremity that may affect
70 gait. Volunteers who did not meet these inclusion criteria were excluded. All
71 participants were notified of the procedures and requirements and were invited
72 to participate by signing an informed consent form. The study and all
73 procedures were approved by the Ethics Committee of the UEL (#217/2012).

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76 2.2 Instrumentation

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78 Data were collected using a waterproof force platform (Bertec
79 Corporation[®], model FP4060-08-2000), with dimensions of 0.6X0.6X0.1 m,
80 sample rate of the acquisition system of 1000 Hz, capacity of $F_z = 5000\text{N}$ and
81 $F_x = F_y = 2500\text{ N}$ and 340 Hz (F_z) and 550 ($F_x = F_y$) of natural frequency with a
82 16-bit A/D converter. The FP was placed in the final third of a 10 meter pool,
83 located in the Aquatic Physical Therapy Center “Prof. Paulo A. Seibert”, with
84 dimensions of 15x13x1.30 m, extent of submersion around 1.20 m and water
85 temperature of 32.5 °C.

86

87 2.3 Procedure

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89 The individuals walked on the platform at a self-selected speed, and
90 were asked to walk onto it with their preferred leg. The test was repeated three
91 times or until three valid data recordings had been collected. A trial was
92 considered successful when only one foot made contact with the platform
93 (Figure 1); trials not meeting these criteria were excluded and another trial was
94 performed. Participants were instructed to walk normally while looking straight
95 ahead and not to look at the platform.

96 Before starting data collection, participants practiced walking across the
97 platform until they were comfortable with the procedure. The gait cycle started
98 with initial foot contact with the force platform and ended when this foot left the
99 platform. For the test-retest reliability, two recordings were performed with a 48-
100 hour interval between them.

101 2.4 Data Processing

102

103 Force plate data were analyzed using a specific routine in Matlab[®] 7.9.0
104 (R2009b, Mathworks, TM), smoothed by a Butterworth low-pass filter of 4th
105 order and cutoff frequency of 5 Hz defined by spectral analysis (Carneiro *et al.*,
106 2012, Hauptenthal *et al.*, 2010b and Miyoshi *et al.*, 2004).

107 The analyzed GRF components were the vertical (Fz), anteroposterior
108 (Fx) and mediolateral (Fy). Maximum and minimum values were selected from
109 the curve profiles to assess the reliability of gait parameters. For the Fz
110 component, the first peak is the response to load (Fz1), the second point is the
111 valley and represents the average support (valley) and the second peak
112 represents the terminal support (Fz2) (White *et al.*, 1999). For the Fx
113 component, the point selected represents the phase-end or maximum
114 propulsion. Two points were considered for the Fy component, the first peak
115 (Fy1) represents a lateral thrust during loading, during which time the foot is
116 moving from a supinated position into pronation and the second peak (Fy2) is a
117 small lateral force often seen during the final push off stage (these parameters
118 are demonstrated in Figure 2) (Miyoshi *et al.*, 2004 and Richards, 2008).
119 Furthermore, the acceptance rates (AR) which correspond to the curve slope
120 during the loading phase were analyzed, calculated by dividing the value of the
121 response to load by the difference between the beginning and the force peak
122 ($Fz1/\Delta t$), as well the propelling charges which are given by dividing the Fz2 by
123 the time difference of the peak and the valley ($\Delta Fz2/\Delta t$) (Sacco *et al.*, 2012).

124 To set the gait cycle, the mean and standard deviation (SD) of the
125 baseline from the Fz data before foot contact were calculated. Thus, the

126 beginning of the gait cycle was defined as the local minimum of the curve,
127 which preceded the moment at which the Fz exceeded the mean value of the
128 baseline added to four standard deviations.

129 Data were normalized by body weight of the subject. An example of a
130 normalized profile curve can be seen in Figure 2. For the reliability analysis, the
131 average value of the three trials of each component was employed (Grainger *et*
132 *al.*, 1983 and Diss, 2001).

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134 *2.5 Statistical analysis*

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136 As the normality assumption for the data was not met, data are
137 presented as median (Md) and quartiles (25-75%). The test-retest reliability was
138 assessed by calculating the intraclass correlation coefficient (ICC) (one-way
139 random effect model) and the agreement analysis proposed by Bland and
140 Altman (1986). An ICC value < 0.4 was considered as poor reproducibility, $0.4 \leq$
141 $ICC \leq 0.75$ indicates fair to good reproducibility and > 0.75 indicates excellent
142 reproducibility (Fleiss, 1986).

143 The Bland-Altman agreement was incorporated with the mean difference
144 (\bar{d}) and their respective 95% confidence intervals (CI), the SD of mean
145 difference (SD of \bar{d}) and the limits of agreement (LA) analyses. In addition the
146 value of the SEM (standard error of measurement) was calculated through the
147 ICC, using the number of errors that can be allocated in the sample; SEM was
148 calculated using the equation $SD \times \sqrt{1 - ICC}$ (Jewell, 2011). In addition, the
149 Wilcoxon test was conducted to compare the forces from the first and the
150 second test in order to evaluate the effect of familiarization on the results.

151 Analyzes were performed in the programs IBM SPSS (Statistical Package for
152 Social Sciences, version 22; Armonk, NY: IBM Corp.) and MedCalc Software
153 bvba (version 15.6.1; Ostend, BE).

154

155 **3. Results**

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157 The values for the vertical component of the GRF were expected for an
158 aquatic activity. **These values (minimal - maximal) ranged from 0.13 - 0.41**
159 **N/BM for the Fz1; 0.03 - 0.37 N/BM for the valley and 0.14 - 0.41 N/BM for the**
160 **Fz2.**

161 The SEM values were low, indicating that the error incorporated in the
162 data was minimal. In relation to the GRF values in the test-retest, statistical
163 differences were found for the Fz1 and Fz2 and no differences for the other
164 parameters (valley, Fx, Fy1, Fy2, AR and PR), which shows that the subjects
165 were able to reproduce the same speed in both tests (Table 1). Despite the
166 differences found for Fz1 and 2, the values for response to load and terminal
167 support, in terms of interquartile range, are alike and moreover, does not seem
168 to be relevant in practice.

169 The test-retest results demonstrated a reliability ranging from poor to
170 excellent for the ICC values and a mean difference close to zero for all
171 parameters. For the Fz and Fx components the reliability values were excellent,
172 while for the rate of acceptance and propulsion was considered good. For the
173 Fy component, the reliability was also good for Fy1 and poor for Fy2, despite
174 this the mean difference was also low, showing that the two measures (test-

175 retest) were similar. Further information about ICC and mean difference can be
176 found in Table 2 and in Figures 3 to 6.

177

178 **4. Discussion**

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180 The aim of this study was to investigate the test-retest reliability of kinetic
181 gait parameters, as measured by a FP, in healthy individuals in water. The
182 results demonstrated variability in the ICC values from 0.24 to 0.87, ranging
183 from poor to excellent. Since the calculation of the ICC in isolation does not
184 provide enough information about the reliability of the measurements, the
185 values generated in the Bland-Altman plots and SEM were used to complement
186 the ICC (Rankin and Stokes, 1998). The identified SEM values in the present
187 study were close to zero, indicating that the number of errors attributed to the
188 sample was low (Jewell, 2011). **When the difference between test and re-test**
189 **was analyzed, it can be observed that there was an increase in Fz 1 and 2. It is**
190 **possible that this may be due to the practice effect, however, the values for**
191 **response to load and terminal support, in terms of interquartile range, are alike**
192 **and moreover, this does not seem to be relevant in practice.**

193 The findings of this current study support the findings of Fortin *et al.*
194 (2008) who evaluated the repeatability of gait parameters individuals with
195 scoliosis. These authors reported that the SEM values found for the three
196 kinetic components of the gait were low. The mean difference values identified
197 in this study by the Bland and Altman plots (Bland and Altman 1986) were close
198 to zero for all items, demonstrating little variation among the data.

199 The component that demonstrated an excellent result for reliability was
200 the Fz, which is similar to previous studies carried out on land, in which the
201 highest values were also found for Fz (Kadaba *et al.*, 1989 and White *et al.*,
202 1999). In the literature, this component is the most frequently used to evaluate
203 GRF in gait (Amadio and Baumann, 2000). Owing to the action of buoyancy and
204 hence the reduced apparent weight, the forces applied to the force platform are
205 also decreased, with a possible reduction in Fz of 60-70% (minimum of 0.13
206 and maximum of 0.41 for Fz1; minimum of 0.03 and maximum of 0.37 for Valley
207 and minimum of 0.14 and maximum of 0.41 for Fz2) compared to on land
208 (minimum of 0.91 and maximum of 1.18 for Fz1; minimum of 0.71 and
209 maximum of 0.95 for Valley and minimum of 0.92 and maximum of 1.23 for
210 Fz2). When buoyancy is added to the drag force in water, a lower speed (about
211 36% compared to on land) can be observed (Barela *et al.*, 2006) and a longer
212 contact time on the FP is generated. Furthermore, lower muscle activity is
213 observed in the water, thus the curve pattern is characterized by less defined
214 peaks (Nakasawa *et al.*, 1994; Miyoshi *et al.*, 2005 and Carneiro *et al.*, 2012).

215 It is mainly through the Fz analysis, that is detected the moment that the
216 heel touch ground (Hreljac and Marshall, 2000; Ghoussayni *et al.*, 2004;
217 O'Connor *et al.*, 2007, Desailly *et al.*, 2009; Asha *et al.*, 2012), allowing a direct
218 relationship between the time of support and the resultant forces of the muscle
219 actions that occur in the lower limbs. As a result, a product of the vector of the
220 GRF is generated and transmitted to the body through the feet, making the
221 vertical component the largest part of the GRF (Winter, 1980). Moreover, it is
222 the component that best represents the GRF with characteristic and consistent
223 graphics, which can provide information about mechanical stress (Piscoya *et*

224 *al.*, 2005). This measure can also characterize joint contact forces, which seem
225 to play an important role in the development of certain musculoskeletal
226 disorders (Piscoya *et al.*, 2005).

227 For the Fx component, excellent ICC values were identified with low
228 mean difference values, which also supports the findings of published studies
229 exploring GRF on land (Kadaba *et al.*, 1989 and Fortin *et al.*, 2008). When
230 analyzing the variation of the Fx component, in the studies of Miyoshi *et al.*
231 (2004) and Orselli and Duarte, (2011), only positive values (anterior direction)
232 were found, which is consistent with the present study which found positive
233 peaks rather than a negative (posterior direction) valley followed by a positive
234 peak (profile curve commonly found on land). This pattern seems appropriate
235 since, by overcoming all water resistance, participants must generate the gait
236 acceleration phase (Miyoshi *et al.*, 2005), thus altering the gait support phase,
237 tilting the body forward and only stepping on the force platform when their lower
238 limb exceeds the longitudinal axis of the body, eliminating the deceleration
239 phase (Miyoshi *et al.*, 2005 and Hauptenthal *et al.*, 2010a). In this current study,
240 only the point of the Fx component (the final peak) was evaluated, this peak
241 represents the maximum propulsion, as the curve profile in water does not allow
242 any other point to be stated with certainty.

243 The Fy component of gait (medial-lateral displacement) demonstrated
244 the lowest reliability values, probably due to the influence of fluid mechanics, it
245 is known that medio-lateral movements are more unstable compared to
246 anteroposterior (Kuo and Donelan, 2010), which changes the movements of the
247 ankle and causes irregular behavior of this joint (Sutherland *et al.*, 1980;
248 Miyoshi *et al.*, 2005). During gait on land, the ankle joint has an important role in

249 supporting the body weight, however, in the aquatic environment, buoyancy
250 decreases the weight of the individual and consequently there is less necessity
251 for the ankle joint to provide support (Miyoshi *et al.*, 2005; Orselli and Duarte,
252 2011; Sutherland *et al.*, 1980).

253 Another possibility for the low reliability of the Fy component may be
254 related to the choice of the peak of the curve that was selected. In water the Fy
255 component does not follow a curve profile as in the case of the other
256 components. The results demonstrated that the Fy component varied across
257 participants, which perhaps suggests that the chosen point on the curve profile
258 may not have been the most suitable, thus increasing overall variability.

259 During gait, the swing phase leg directly influences the medio-lateral
260 vector of GRFs due to displacement of the body center of mass to the side of
261 the stance leg. In addition, the turbulence generated by the oscillating limb and
262 the reduction of muscular activity in the water can interfere with the amplitude
263 value of Fy (Sutherland *et al.*, 1980; Barela *et al.*, 2006 and Lin *et al.*, 2014).
264 The range of ICC values of Fy demonstrated poor to good reliability (between
265 0.24 and 0.68), which has been observed by others on land, previous authors
266 have attributed this high variability to intrinsic factors. According to Redfern and
267 Schumann (1994), the high variability may be associated with the positioning of
268 the foot, which varies between individuals and also between each trial.

269 Furthermore, there are the effects of drag force, buoyancy and turbulent
270 flow, which can promote variability in the Fy component (Fy1 and Fy2) (Miyoshi
271 *et al.*, 2005). The reliability values for the acceptance and propulsion rate were
272 high, which may be explained by some physical properties of water such as

273 drag force, as well as the lower speed that promotes a decrease in gait kinetic
274 parameters (Kyröläinen *et al.*, 2001 and Barela *et al.*, 2006).

275 In this study the speed was not standardized, which could be a limiting
276 factor, however no differences were found in the duration of the stance phase
277 when comparing the test and retest (Lafuente *et al.*, 2000 and Kyröläinen *et al.*,
278 2001). In addition, the data did not present a normal distribution, but they were
279 analyzed by Bland and Altman plots and ICC, which may have introduced some
280 bias in to the results. Thus, future studies should standardize the gait speed of
281 the participants and evaluate simultaneously kinematics and joint moments.

282 **5. Conclusion**

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284 It is important to be able demonstrate the reliability of the assessment of
285 the components of gait for research and clinical practice. Through accurate
286 knowledge of the GRFs during different exercises, exercise prescription can be
287 made more specific and appropriate for the patient. The test-retest reliability of
288 the kinetic gait parameters of healthy individuals, in the aquatic environment,
289 presented poor to excellent reliability. The vertical and anteroposterior
290 components of gait demonstrated high ICC values, and the vertical component
291 was the most reliable, **although some practice effect may have influenced this**
292 **measure**; however, caution should be taken when evaluating the medial-lateral
293 component, as its reliability was low.

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300 **References**

301

302 Amadio AC, Baumann W. Aspects of methodology to determine the internal
303 forces of the locomotor system. *Braz J Biomech* 2000;1:7-14.

304

305 Barela AMF, Stolf SF, Duarte M. Biomechanical characteristics of adults
306 walking in shallow water and on land. *J Electromyogr Kinesiol* 2006;16:250-6.

307

308 Bland JM, Altman D. Statistical methods for assessing agreement between two
309 methods of clinical measurement. *Lancet* 1986;327:307-10.

310

311 Carneiro LC, Michaelsen SM, Roesler H, Hauptenthal A, Hubert M, Mallmann E.
312 Vertical reaction forces and kinematics of backward walking underwater. *Gait*
313 *Posture* 2012;35:225-30.

314

315 De Asha AR, Robinson MA, Barton GJ. A marker based kinematic method of
316 identifying initial contact during gait suitable for use in a real-time visual
317 feedback application. *Gait Posture* 2012;36:650-2.

318

319 Desailly E, Daniel Y, Sardain P, Lacouture P. Foot contact event detection
320 using kinematic data in cerebral palsy children and normal adults gait. *Gait*
321 *Posture* 2009;29:76-80.

322

323 Diss CE. The reliability of kinetic and kinematic variables used to analysis
324 normal running gait. *Gait Posture* 2001;14:98-103.

325

326

327 Donoghue OA, Shimojo H, Takagi H. Impact forces of plyometric exercises
328 performed on land and in water. *Sports Health* 2011;3:303-9.

329

330 Duarte M, Freitas SMSF. Revision of posturography based on force plate for
331 balance evaluation. *Br J Phys Ther* 2010;14:183-92.

332

333 Fleiss JL, 1986. *The design and analysis of clinical experiments*. New York:
334 Wiley.

335

336 Fontana HB, Haupenthal A, Ruschel C, Hubert M, Ridehalgh C, Roesler H.
337 Effect of gender , cadence, and water immersion on ground reaction forces
338 during stationary running. *J Orthop Sports Phys Ther* 2012;42:437-43.

339

340 Fontana HB, Haupenthal A, Ruschel C, Pizzolatti ALA, Cerutti PR, Roesler H.
341 Comparison of ground reaction forces between in-place and forward water
342 running at two levels of immersion. In: Vilas-Boas JP, Machado L, Kim W,
343 Veloso AP, Alves F, Fernandes RJ, Conceição F editors. *Biomechanics in*
344 *Sports* 29. Porto: Rev Port Cien Desp 2011;11:495-8.

345

346 Fortin C, Nadeau S, Labelle H. Inter-trial and test–retest reliability of kinematic
347 and kinetic gait parameters among subjects with adolescent idiopathic scoliosis.
348 *Eur Spine J* 2008;17:204-16.

349

350 Grainger J, Norman C, Winter D, Bobet J. Day to day reproducibility of selected
351 biomechanical variables calculated from film data. In: Matsui H, Kobayashi K,
352 editors. Biomechanics VIII A & B. Champaign: Human Kinetic Publishers,
353 1983:1239-47.

354

355 Ghoussayni S, Stevens C, Durham S, Ewins D. Assessment and validation of a
356 simple automated method for the detection of gait events and intervals. *Gait*
357 *Posture* 2004;20:266-72.

358

359 Hamill J, McNiven SL. Reliability of selected ground reaction force parameters
360 during walking. *Hum Mov Sci* 1990;9:117-31.

361

362 Harrison RA, Bulstrode S. Percentage weight-bearing during partial immersion
363 in the hydrotherapy pool. *Physiother Pract* 1987;3:60-3.

364

365 Harrison RA, Hillman M, Bustrode S. Loading of the lower limb when walking
366 partially immersed: implications for clinical practice. *Physiotherapy* 1992;78:
367 164-6.

368

369 Hauptenthal A, Fontana HB, Ruschel C, Roesler H, Borgatto AF. Prediction of
370 ground reaction force during water immersion running. *Fisioter Pesqui*
371 2010a;17:253-8.

372

373 Haupenthal A, Ruschel C, Hubert M, Fontana HB, Roesler H. Loading forces in
374 shallow water running in two levels of immersion. J Rehabil Med 2010b;42:664-
375 9.

376

377 Haupenthal A, Ruschel C, Hubert M, Fontana HB, Roesler H. Ground reaction
378 force as a subsidy for prescribing aquatic exercises: case study. Fisioter Mov
379 2010c;23:303-10.

380

381 Haupenthal A, Fontana HB, Ruschel C, Santos DP, Roesler H. Ground reaction
382 forces in shallow water running are affected by immersion level, running speed
383 and gender. J Sci Med Sport 2013;16:348-52.

384

385 Hreljac A, Marshall RN. Algorithms to determine event timing during normal
386 walking using kinematic data. J Biomech 2000;33:783–6.

387

388 Jewell, DV. Guide to evidence-based physical therapist practice. 2nd ed.
389 Sudbury: Jones e Bartlett Learning, 2011.

390

391 Kadaba MP, Ramakrishnan HK, Wootten ME, Gainey J, Gorton G, Cochran
392 GV. Repeatability of kinematic, kinetic, and electromyographic data in normal
393 adult gait. J Orthop Res 1989;7:849-60.

394

395 Kuo AD, Donelan JM. Dynamic principles of gait and their clinical implications.
396 Phy Ther 2010;90:157-74.

397

- 398 Kyröläinen H, Belli A, Komi PV. Biomechanical factors affecting running
399 economy. *Med Sci Sports Exerc* 2001;33:1330-7.
400
- 401 Lafuente R, Belda JM, Sánchez-Lacuesta J, Soler C, Poveda R, Prat J.
402 Quantitative assessment of gait deviation: contribution to the objective
403 measurement of disability. *Gait Posture* 2000;11:191-8.
404
- 405 Lexell JE, Downham DY. How to assess the reliability of measurements in
406 rehabilitation. *Am J Phys Med Rehabil* 2005;84:719-23.
407
- 408 Lin YC, Gfoehler M, Pandy MG. Quantitative evaluation of the
409 major determinants of human gait. *J Biomech* 2014;47:1324-31.
410
- 411 Miyoshi T, Shirota T, Yamamoto S, Nakazawa K, Akai M. Lower limb joint
412 moment during walking in water. *Disabil Rehabil* 2003;25:1219-23.
413
- 414 Miyoshi T, Shirota T, Yamamoto S, Nakazawa K, Akai M. Effect of the walking
415 speed to the lower limb joint angular displacements, joint moments and ground
416 reaction forces during walking in water. *Disabil Rehabil* 2004;26:724-32.
417
- 418 Miyoshi T, Shirota T, Yamamoto S, Nakazawa K, Akai M. Functional roles of
419 lower-limb joint moments while walking in water. *Clin Biomech* 2005;20:194-
420 201.
421

- 422 Nakazawa K, Yano H, Miyashita M. Ground reaction forces during walking in
423 water. In: Miyashita M, Mutoh Y, Richardson AB, eds. *Medicine and Science in*
424 *Aquatic Sports*. Med Sport Sci, Switzerland: Karger 1994;39:28-34.
425
- 426 O'Connor CM, Thorpe SK, O'Malley MJ, Vaughan CL. Automatic detection of
427 gait events using kinematic data. *Gait Posture* 2007;25:469-74.
428
- 429 Orselli MIV, Duarte M. Joint forces and torques when walking in shallow water.
430 *J Biomech* 2011;44:1170-5.
431
- 432 Piscoya JL, Fermor B, Kraus VB, Stabler TV, Guilak F. The influence of
433 mechanical compression on the induction of osteoarthritis-related biomarkers in
434 articular cartilage explants. *Osteoarthr Cartil* 2005;13:1092-9.
435
- 436 Portney LG, Watkins MP. *Reliability of Measurements*. In: Prentice-Hall, editors.
437 *Foundations of clinical research applications to practice*. 3rd ed. New Jersey:
438 Upper Saddle River; 2000:77-96.
439
- 440 Rankin G, Stokes M. Reliability of assessment tools in rehabilitation: an
441 illustration of appropriate statistical analyses. *Clin Rehabil* 1998;12:187-99.
442
- 443 Redfern MS, Schumann T. A model of foot placement during gait. *J*
444 *Biomech* 1994;27:1339-46.
445

- 446 Richards J. Ground reaction forces, impulse and momentum. In: Jim Richards
447 editor. Biomechanics in Clinic and Research. London: Churchill Livingstone,
448 2008:35-49.
- 449
- 450 Sacco IC, Sartor CD, Cacciari LP, Onodera AN, Dinato RC, Pantaleão E Jr.
451 Effect of a rocker non-heeled shoe on EMG and ground reaction forces during
452 gait without previous training. *Gait Posture* 2012;36:312-5.
- 453
- 454 Sutherland DH. The evolution of clinical gait analysis part III - Kinetics and
455 energy assessment. *Gait Posture* 2005;21:447-61.
- 456
- 457 Sutherland DH, Cooper L, Daniel D. The role of the ankle plantar flexors in
458 normal walking. *J Bone Joint Surg Am* 1980;62:354-63.
- 459
- 460 Veilleux LN, Rauch F, Lemay M, Ballaz L. Agreement between vertical ground
461 reaction force and ground reaction force vector in five common clinical tests. *J*
462 *Musculoskelet Neuronal Interact* 2012;12:219-23.
- 463
- 464 White R, Agouris I, Selbie RD, Kirkpatrick M. The variability of force platform
465 data in normal and cerebral palsy gait. *Clin Biomech* 1999;14:185-92.
- 466
- 467 Winter DA. Overall principle of lower limb support during stance phase of gait. *J*
468 *Biomech* 1980;13:923-7.