



## HOMER analysis of the water and renewable energy nexus for water-stressed urban areas in Sub-Saharan Africa

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24 Africa and assess whether the solutions are cost-effective. The analysis shows investment in  
25 renewable technologies is cost-effective when the true cost of electricity or average days of  
26 power outages per year are considered. Integration of photovoltaic panels, a wind turbine and  
27 internal combustion engine fuelled by biogas produced by anaerobic digestion can cover  
28 between 33% and 55% of the electricity demand of the basic wastewater facility, at a  
29 levelised cost of energy lower than the true cost of electricity. In the case of water reuse, the  
30 techno-economically viable solutions identified by HOMER can cover 13% of energy needs.  
31 Finally, we discuss how the proposed solutions could provide a large contribution to socio-  
32 political security, in both domestic and cross-border contexts.

33 **Keywords:** *water energy nexus; renewable technologies; wastewater treatment; Sub-Saharan*  
34 *Africa, socio-political security; HOMER*

35

### 36 **Nomenclature**

37	C	cost (\$)
38	CHP	combined heat and power
39	COD	chemical oxygen demand
40	COE	cost of energy (\$/kWh)
41	CRF	capital recovery factor
42	E	Energy (kWh)
43	i	real interest rate
44	ICE	internal combustion engine
45	N	number of year
46	NPC	net present cost
47	PE	population equivalent
48	PV	photovoltaic
49	R	Lifetime (year)
50	SS	suspended solid (kg/person/year)

### 51 **Subscripts**

52 *ann,tot* total annualised  
53 *def* deferrable loads  
54 *el* electrical  
55 *grid, sales* sold to the grid  
56 *proj* project

57

58 **Highlights**

- 59 • The benefits of integrating renewables in wastewater treatment plants are studied.
- 60 • A case study in Sub Saharan Africa is analysed with the aid of HOMER.
- 61 • The investment is cost-effective if the real cost of electricity is considered.
- 62 • Renewables can cover up to 55% of electricity demand for a conventional facility.
- 63 • In a wastewater treatment facility with water reuse this reduces to 13%.

64

## 65 **1. Introduction**

66 The most significant challenges currently faced by Sub-Saharan Africa arise from or intersect  
67 with water issues (*Freitas, 2013*). According to the World Health Organization, over 40% of  
68 the population in Sub-Saharan Africa do not have access to safe drinking water. Water is not  
69 only scarce, but also of poor quality; 45% of the population only have access to shared and  
70 inadequate sanitation facilities. Indeed, 30% of people only gained access to improved  
71 sanitation in recent years, and Sub-Saharan Africa missed the 2015 Millennium Development  
72 Goal sanitation target: “halve the proportion of the population without sustainable access to  
73 basic sanitation” (*Unicef, 2015*). Moreover, climate change, the growing population and  
74 increasing urbanisation act as stress multipliers. Assessment Report 5 of the  
75 Intergovernmental Panel of Climate Change (*IPCC, 2014*) provides a clear picture of the  
76 effects of climate change: the medium-risk scenario predicts an increase in the land  
77 temperature of most regions of Africa of more than 2°C, particularly in arid regions. Climate  
78 change will reduce water availability, increase hydro-climatic variability in both space and  
79 time and raise the risk of extreme weather events. A reduction in precipitation combined with  
80 increased temperatures is likely reduce crop production and threaten food security over the  
81 long-term, especially as Sub-Saharan Africa mainly relies on rain-fed agriculture.

82 A recent report by Hove et al. (2013) predicted the population of Sub-Saharan Africa  
83 will almost double by 2050. Since the early 1970s, Sub-Saharan Africa has experienced the  
84 highest rate of urban population growth worldwide, averaging up to 5% per year (*Todaro and*  
85 *Smith, 2012*). According to Nyenje et al. (2010), monitoring reports indicate the populations  
86 of the mega-cities in Sub-Saharan Africa are rapidly increasing, and therefore, so is the total  
87 amount of wastewater produced. Less than 30% of wastewater is treated in sewage treatment  
88 plants, while the remainder is disposed of via onsite sanitation systems and eventually  
89 discharged into groundwater. The total amount of wastewater produced in Sub-Saharan

90 African megacities can be as high as 10–50% of the total precipitation entering these urban  
91 areas, which is considerable since precipitation is the most important - if not only –  
92 wastewater diluting agent. Recent literature has highlighted the increasing levels of pollution  
93 in African water bodies (*Ali, 2011; Scheren et al., 2000*), illustrating the severe impact of  
94 effluents on downstream water. Therefore, it is imperative to treat wastewater before  
95 discharging it into the drainage basin, and if combined with water reuse, wastewater  
96 treatment may provide a solution to satisfy the increasing water demands of Sub-Saharan  
97 Africa. Numerous scientists and policy makers (*Therewowda et al., 2016*) are exploring the  
98 wastewater treatment issue and also consider the reuse of treated wastewater as a viable,  
99 interesting option. Energy requirements are a major barrier to the implementation of  
100 wastewater treatment and reuse strategies: this is a timely topic that urgently needs to be  
101 addressed by the energy sector. For the first time, the 2016 World Energy Outlook will  
102 explore the energy needs of the global water industry, including wastewater treatment  
103 facilities (IEA, 2016).

104 Sub-Saharan Africa is the most electricity-poor region in the world; according to the  
105 2015 World Energy Outlook access database (*WEO, 2015*), the average electrification rate is  
106 35%, with urban and rural electrification rates of 59% and 17%, respectively. In this context,  
107 it would be difficult to meet the additional demands for energy arising from wastewater  
108 treatment facilities. Renewable energy technologies, and in particular micro-grids, represent a  
109 possible solution. According to the recent World Bank Energy Report (*The World Bank,*  
110 *2015*), Sub-Saharan Africa could increase its current energy capacity by up to 170 GW  
111 through the introduction of small installations, such as combined heat-and-power systems and  
112 production of biofuels.

113 The present work investigates the energy needs of wastewater treatment and  
114 reclaimed water reuse facilities. We aimed to assess the benefits of integrating renewable

115 energy technologies into wastewater treatment facilities situated in urban areas of water-  
116 stressed river basins. In particular, we identify the optimal combinations of renewable energy  
117 technologies for a wastewater treatment facility without or with water reuse capacity situated  
118 in a given urban area of Sub-Saharan Africa under three different scenarios, and analyse  
119 whether the solutions are cost-effective. The work assumes a number of served inhabitants of  
120 10,000 (equal to about 11,000 Population Equivalent, PE). Although a decentralised  
121 wastewater treatment facility typically serves from 1,000 to 10,000 PE (*Libralato et al.,*  
122 *2012*), the authors agree with *Gikas and Tchobanoglous (2009)* about the difficulty of  
123 attributing a precise threshold. Here, we embrace the main concept of decentralised systems,  
124 in that the raw wastewater is treated next to the source, in line with the concept of  
125 decentralised energy production, next to the user. For the present work, the decentralised  
126 facility could even be thought of as being in parallel to the central system, just as the energy  
127 production from renewable sources occurs in parallel to the main electricity grid. The urban  
128 area is assumed to have a wastewater collection system (which is not always the case), either  
129 through pipes or tanks. For water reuse applications, the standard requirements vary  
130 according to the specific reuse of the treated water. The present paper focuses on the reuse of  
131 water for agricultural irrigation, which is of particular interest since more than 70% of the  
132 freshwater used worldwide is used for agricultural irrigation (*Capra and Scicolone, 2007;*  
133 *Lazarova, 2012*). The paper assesses the proposed integrated solutions from a techno-  
134 economic point of view using HOMER, a software tool specifically developed for optimal  
135 analysis of hybrid micro-generation systems (*Lambert et al., 2006*).

136 The exploration of the results is followed by a post-HOMER analysis of how the  
137 proposed solution can address security problems and help to mitigate cross-border conflicts.  
138 Any initiatives that reduce water pollution and address the problem of water scarcity could  
139 act as a conflict relief, given that 75% of the water resources in Sub-Saharan Africa are

140 concentrated in eight major transboundary river basins. Therefore, any usage of cross-  
141 boundary water, including that to satisfy increasing energy demand, can represent a potential  
142 source of conflict between the states through which these rivers flow (*Chellaney, 2011*). The  
143 Nile river basin, which extends over 11 countries, provides a meaningful example of such  
144 cross-border security issues. Upstream countries such as Ethiopia are less industrialised, yet  
145 in recent years their needs for water and energy, the latter of which is mainly produced by  
146 hydroelectric plants, have increased. Downstream countries, such as Egypt, have also faced  
147 increased water and energy demands due to growth of both the population and energy  
148 intensive industry, creation of desalination plants and changes in lifestyle (*Sowers, 2014*).  
149 Therefore, any water and energy issues that involve the use of this shared water body can  
150 rapidly create tensions, as demonstrated by the construction of a new dam on the river Nile in  
151 Ethiopia, the Grand Renaissance Dam, which could threaten the water supply of downstream  
152 countries.

153 In section 2 of this paper, we discuss the wastewater and renewable energy nexus;  
154 section 3 describes the methods adopted for the HOMER analysis; section 4 details the  
155 system modelled; and section 5 discusses the solutions generated by the simulation. Finally,  
156 through a post-HOMER analysis, section 6 addresses the relevance of the proposed technical  
157 solutions in the context of the security background of the region.

158

## 159 **2. Wastewater and energy nexus**

160 This section provides an overview of the interactions between wastewater and energy, with  
161 the aim of clarifying this nexus and providing evidence of the knowledge gaps that justify the  
162 present work. A growing number of studies are focusing on the wastewater and energy nexus  
163 (*Wells et al., 2014*), since understanding the interactions between wastewater and energy will  
164 help to implement more effective and efficient infrastructure systems (*Plappally, 2012*).

165 Wastewater and energy are closely linked: energy is necessary for wastewater distribution,  
166 usage and treatment; and wastewater contains energy in different forms: kinetic, potential,  
167 and thermal and chemically-bound energy (*Lazarova et al., 2012*). The kinetic energy of  
168 water depends on its flow rate and can be exploited through turbines (*Gallagher et al., 2015*),  
169 Archimedean screws or water wheels. Potential energy is limited in the contribution that it  
170 can provide, and is generally neglected, while the thermal energy content is expected to have  
171 interesting applications for space heating (*Nowak et al., 2015*). Chemically-bound energy has  
172 recently emerged as an energy form that could potentially be used to meet the entire energy  
173 demands of conventional wastewater treatments (*Hao et al., 2015*). The value of chemically-  
174 bound energy can be calculated as a function of the organic content (i.e. chemical oxygen  
175 demand), and is roughly equal to 3.49 kWh per kg of chemical oxygen demand. To provide  
176 an idea of the amount of energy that can be potentially produced from wastewater, a recent  
177 study conducted on a German wastewater utility calculated values of 16 kWh/(person year)  
178 for potential energy, 6 kWh/(person year) for kinetic energy, 509 kWh/(person year) for  
179 thermal energy and 146 kWh/(person year) for chemically-bound energy (*Lazarova et al.,*  
180 *2012*).

181 Anaerobic digestion combined with Combined Heat and Power, CHP, plants is  
182 currently the most widely-applied technology for electricity and thermal production (*Silvestre*  
183 *et al., 2015*); however, the percentage of chemical energy that can be recovered is lower than  
184 the energy needs of the facility. The current trend is to design wastewater treatment facilities  
185 that reduce (*Li et al., 2016*) or recover energy (*Mo and Zhang, 2013*) together with chemicals,  
186 such as nitrogen and phosphorous, that can be used as agricultural fertilisers (*Chen and Chen,*  
187 *2013*). This concept is of particular interest for less developed countries, like Sub-Saharan  
188 Africa where electricity access in some regions is lower than 40% and the cost of fertilisers is  
189 higher than in other regions of the world (*Morris, 2007*). Wastewater is a valuable resource

190 since 99.5% of its volume is water; therefore, its reuse furthermore reduces the discharge of  
191 wastewater into water bodies (*Morera et al., 2016*). Although the energy requirements are  
192 generally high, wastewater reuse represents a solution for areas where the water system is  
193 already under stress due to rapid urbanisation and a high risk of extreme events in response to  
194 climate change.

195 Treating and reusing wastewater in Sub-Saharan Africa requires the identification of  
196 sustainable solutions to satisfy the energy needs required for these processes. Two possible  
197 pathways exist: i) to introduce wastewater treatment facilities that are capable of recovering  
198 or even producing energy, and ii) to apply renewable technologies to exploit the advantages  
199 of co-optimised investment in water and renewable energy.

200 The *first pathway* is the most promising but requires additional effort from research  
201 and industry, since technologies that are able to significantly reduce and fully satisfy the  
202 energy needs of a wastewater treatment facility are not yet deployable at full scale; indeed,  
203 some of these technologies are only in the pre-commercial phase. With respect to this  
204 promising pathway and water reuse, it is worth mentioning anaerobic membrane bioreactors  
205 and microbial electrolysis cells. Termed AnMBR, this option is an example of an energy  
206 generation solution based on a combination of anaerobic digestion and membrane separation,  
207 which provides a high quality of effluent. AnMBRs have a small footprint, thanks to their  
208 ability to contain a high concentration of solids. Although several aspects such as membrane  
209 fouling still need to be investigated further, the main advantage of AnMBRs is their efficient  
210 recovery of resources, including nutrients such as nitrogen and phosphorous (*Shoener et al.,*  
211 *2014*). Microbial electrolysis cells, a type of microbial fuel cell, are currently being assessed  
212 for municipal water and wastewater treatment markets in the EU, and it is expected that the  
213 first generation of microbial electrolysis cell electrolyzers will be ready within 1-4 years  
214 (*Escapa et al., 2014*). The use of microbial electrolysis cells for wastewater treatment was

215 first proposed in 1991 and several studies have been performed since (*Gil-Carrera, 2013*). A  
216 12 month pilot project recently carried out in the UK reported promising results (EC, 2013).  
217 Although microbial electrolysis cell can remove 0.14 kg chemical oxygen demand/m<sup>3</sup>/day  
218 compared with the 0.2-2 kg chemical oxygen demand/m<sup>3</sup>/day removed by current activated  
219 sludge systems, microbial electrolysis cells also offer the advantage of producing hydrogen.

220 The *second pathway* represents a goal that is achievable in the short-term, since  
221 renewable energy sources have high potential, especially in Africa, and most of the  
222 technologies are at a mature phase. In this pathway, renewable technologies can be  
223 introduced into decentralised and semi-decentralised wastewater treatment facilities, in order  
224 to help the electricity grid to satisfy the energy demand of wastewater treatment and reuse.  
225 While numerous studies have assessed the benefits and problems associated with introducing  
226 renewable technologies in developing countries (*Chauhan and Saini, 2016*), to the best of the  
227 authors' knowledge, none have focused on satisfying the energy demands of a wastewater  
228 treatment facility. Furthermore, research into the wastewater and renewable energy nexus has  
229 mainly focused on a single wastewater treatment technology that also provides a source of  
230 renewable energy, like anaerobic digesters, while very few studies (*Schäfer et al., 2015*) have  
231 contributed to the discussion on the integration of different renewable technologies and  
232 wastewater treatment facilities and their management. The present work focuses on this latter  
233 approach, taking a hypothetical wastewater system in Sub-Saharan Africa as a reference.  
234 Furthermore, this study provides an insight into the reasons for and impact of such a solution  
235 in the context of the socio-political security of river basin areas in Africa.

236 The authors' contribution mainly comprises four aspects: i) analysis of the integration  
237 of three different renewable energy technologies (i.e. solar photovoltaic, internal combustion  
238 engines fuelled by biogas, wind turbines) to satisfy the electricity demand of wastewater  
239 treatment facilities in arid regions of less developed countries; ii) cost and benefit analysis of

240 introducing renewable technologies into wastewater treatment facilities in less developed  
241 countries, by comparing the net present cost and the levelised cost of energy of the renewable  
242 technologies with conventional energy generation; iii) assessment of the potential coverage of  
243 the electrical loads from local renewable sources; and iv) a discussion of the impact of  
244 applying the proposed technical solutions on human security on the wider scale.

245

### 246 **3. Methods**

247 In the literature, varied materials and methods have been considered to explore the water and  
248 energy nexus. Several studies have been based on life cycle analysis accounting for  
249 emissions, water and land impact on a “cradle to grave” basis, considering all stages from  
250 raw material extraction, manufacturing, to end-life disposal. *Shao et al. (2013)* used life cycle  
251 analysis to assess embodied energy for ecological wastewater treatment by tracing back each  
252 stage of the production process. *Pfister et al. (2011)* employed life cycle analysis to assess  
253 water production by different power production technologies. *Li et al. (2012)* performed an  
254 input-output hybrid life cycle analysis to assess the water consumption and carbon footprint  
255 of wind power generation facilities in China. Other studies have analysed the water and  
256 energy nexus using supply chain analysis, including *Pan et al. (2012)* who investigated the  
257 water and energy nexus of coal power plants in China. *Shao and Chen (2015, 2016)*  
258 compared the resource utilization efficiency of a constructed wetland wastewater treatment  
259 system, using an input output analysis to account for embodied exergy and energy.

260 The approach used in this paper differs from previous studies. Our aims were to  
261 assess the benefits of incorporating renewable energy technologies into wastewater treatment  
262 facilities, and by identifying the optimal configuration of renewable technologies. Rather than  
263 analysing the ecological footprint of a specific wastewater treatment process, this work seeks  
264 solutions that employ local renewable energy sources to satisfy the electrical demand of

265 wastewater treatment plants in arid and electricity-poor regions, to reduce the carbon  
266 footprint of the plants. The analysis is based on HOMER, a software package developed by  
267 the US National Renewable Energy Laboratory, which enables comparison of different  
268 energy systems on the basis of their technical and economic merit (*Lambert et al., 2006*).

269 HOMER is a simulation and optimization toolbox that models the hourly  
270 performances of different system configurations, allowing the user to identify the optimal  
271 combination that satisfies the technical constraints at the minimum net present cost. The  
272 software is intended to assess micro-generation systems that generate electricity and heat to  
273 serve a nearby load. Such systems can be isolated or connected in parallel to the grid, and be  
274 composed of renewable and/or conventional technologies (i.e. diesel engines) and storage  
275 technologies. HOMER can model any micro-generation system, such as photovoltaic units,  
276 wind turbines and Combined Heat and Power units, and provides a wide library of self-  
277 defined systems that can be chosen by the modeller. The software has been developed to  
278 address the challenges generally encountered in the simulation of micro-generation systems,  
279 such as the large number of design options and the uncertainty of key parameters, and allows  
280 the user to develop a sensitivity analysis by performing multiple optimizations of the design  
281 systems under a range of defined parameters.

282 The simulation process determines the feasibility of the specific configuration,  
283 demonstrating if the proposed solution is able to serve the electrical and thermal loads and  
284 satisfy the constraints imposed, and estimates the total cost of installing and operating the  
285 system. In the case of renewable energy technologies, HOMER can help to decide what to do  
286 with the surplus electricity from renewable sources in times of excess and how best to  
287 generate additional power. HOMER uses a cost-based dispatch logic regardless of  
288 configuration. It determines whether renewable energy sources are able to satisfy the load,

289 and if not, identifies the optimal dispatchable system that can meet demand on the basis of  
290 minimisation of the fixed and marginal cost.

291 This analysis of the wastewater and renewable energy nexus in the context of water  
292 treatment and reuse is based on a typical wastewater treatment facility in a Sub-Saharan  
293 urban area. Selection of a specific location is necessary to define the resources available for  
294 renewable energy production. Bahir Dahr, an urban town in north-western Ethiopia, has been  
295 selected as a reference. The area has its own pipe sewage system and is currently suffering  
296 from severe water pollution mainly due to unsustainable industrial and agriculture practices,  
297 the effects of which have been aggravated by climate change and population growth (*Wosnie  
298 and Wondie, 2014*).

299 In this paper we refer to a typical wastewater treatment facility, which is generally  
300 composed of different sections designed for a specific function, as shown in Fig. 1. A  
301 primary treatment (pre-treatment) section removes solid materials, and wastewater is  
302 screened, measured and the main debris removed. A secondary treatment section removes  
303 organic matter, as well as the nitrogen and phosphorous content. This section consists of a  
304 primary clarifier, in which organic matter is physically removed, combined with a biological  
305 treatment, and represents the core of the system. Frequently, a secondary clarifier follows the  
306 primary clarifier. The sludge coming from the first and second clarifiers is generally sent to  
307 an anaerobic digester for the production of biogas to generate electricity and thermal energy.  
308 Finally, tertiary treatments can be added to improve the quality of the treated wastewater,  
309 especially when the reuse is intended for drinking or irrigation. The biological treatment is  
310 generally a bioreactor that converts the biological oxygen demand to bacterial biomass. The  
311 most widespread biological treatment used in commercial plants is conventional activated  
312 sludge technology.

313           The choice of the biological treatment strongly depends on the quality of the influent  
314 and effluent. The present paper analyses two different cases: i) the use of a conventional  
315 activated sludge system in a standard wastewater treatment facility, and ii) the use of a  
316 membrane bioreactor to produce treated wastewater suitable for reuse in irrigation. Although  
317 membrane bioreactors have only been developed at pilot scale, they have been already  
318 experimented with in Africa (*Skouteris, 2014*) and the technology has been demonstrated to  
319 provide a quality of effluent suitable for reuse as irrigation water. Moreover, membrane  
320 bioreactors are also characterised by the highest energy requirements, providing the worst-  
321 case scenario in terms of energy demand (*Krzeminski et al., 2012*). The techno-economic  
322 analysis was performed in three main steps, as described below.

323   ***Step 1: Definition of the daily and seasonal water profiles of the wastewater treatment***  
324 ***facility serving the population***

325 Starting with the total withdrawal per capita reported in *FAO (2015)*, seasonal and daily  
326 variations have been assumed. In the area under analysis, three main seasons can be  
327 considered: a rainy season from March to August; a transition season from September to  
328 October characterized by low rainfall, and a drought season from November to April  
329 (*Mushir, 2012*). The daily trend has been derived from the literature and scaled according to  
330 the average seasonal water withdrawal value (*Quasim, 1998*). The water flow trends  
331 experienced by the facility are illustrated in Figure 2a, with the wastewater facility assumed  
332 to treat 793,356 m<sup>3</sup> of water per year.

333           Since the treatments for water reuse strongly depend on the characteristics of the  
334 wastewater, the main parameters of the influent wastewater have been identified from the  
335 available literature, and are summarized in Table 1.

336   ***Step 2: Definition of energy load profiles for the wastewater treatment facility***

337 Once the daily profiles of the wastewater to be treated have been defined, the electricity  
338 demand must be calculated. The amount of energy required by different wastewater treatment  
339 plants varies widely, but the average energy demand, expressed in kWh per m<sup>3</sup> of treated  
340 wastewater, can be estimated according to the technology chosen (*Logan, 2008*).

341 The wastewater treatment facility under analysis follows the scheme reported in Fig.  
342 1. In the water reuse case, the conventional activated sludge system is replaced with a  
343 membrane bioreactor. Average energy demands of 0.5 kWh/m<sup>3</sup> (*Bodik and Kubaská, 2013*)  
344 and 3.7 kWh/m<sup>3</sup> (*Skouteris et al., 2014*) have been considered for the facilities based on the  
345 conventional activated sludge system and membrane bioreactor, which correspond to  
346 approximately 402 MWh/year and 2,945 MWh/year, respectively. Figure 2b shows the  
347 electrical profiles; it is worth noting that calculation of hourly values is necessary to account  
348 for the variability of intermittent renewable energy sources.

349 ***Step 3: Techno-economic assessment of various renewable energy solutions for the***  
350 ***wastewater treatment facility using HOMER***

351 Once the electrical energy profiles had been defined, the HOMER software tool was used to  
352 assess the suitability of various renewable energy systems. HOMER identifies the best  
353 configuration on the basis of the minimum net present cost (Eq. 1), which represents the life  
354 cycle cost of the system. In contrast to a life cycle costing approach (*Shao et al., 2016*), the  
355 life-cycle cost provided by HOMER considers the cost of installing and operating the system  
356 over its lifespan, and includes all costs and revenues, with future cash flow discounted to the  
357 present. It is possible to specify the discount and inflation rate, as well as the project lifetime;  
358 a project lifetime of 25 years, annual discount rate of 8% and expected inflation rate of 2%  
359 were assumed. The net present cost includes the cost of the initial capital, cost of replacing  
360 components, maintenance and all the operating costs during the lifetime of the project. In the  
361 net present cost, costs are positive and revenues are negative, having the opposite sign of the

362 net present value. All the costs are in US dollars. The net present value, and therefore the net  
 363 present cost, is one of the most widely-used capital budgeting methods for evaluating  
 364 investment projects.

$$365 \quad NPC = \frac{\sum C_{ann,tot}}{CRF \cdot R_{proj}} \quad (1)$$

366 where  $C_{ann,tot}$  is the total annualized cost (\$/yr),  $CRF$  is the capital recovery factor, and  $R_{proj}$  is  
 367 the project lifetime expressed in years. The  $CRF$  is the figure generally used in capital  
 368 budgeting to calculate the present value of an annuity (Eq.2):

$$369 \quad CRF(i, N) = \frac{i(1+i)^N}{(1+i)^N - 1} \quad (2)$$

370 where  $i$  is the real interest rate and  $N$  is the number of years considered for recovery of the  
 371 investment.

372 The life cycle cost is used to calculate the cost of energy (Eq. 3), which represents the  
 373 levelized cost of energy, defined as the ratio between the total annualized cost,  $C_{ann,tot}$ , of the  
 374 system and the energy produced. Cost of energy is a useful parameter that is generally  
 375 applied to compare different energy technologies (*Peterson and Fabozzi, 2012*), and is  
 376 calculated as shown in (Eq. 3).

$$377 \quad COE = \frac{C_{ann,tot}}{E_{prim} + E_{def} + E_{grid,sales}} \quad (3)$$

379 where  $E_{prim}$  and  $E_{def}$  are the total amount of primary and deferrable load, respectively, and  
 380  $E_{grid,sales}$  is the energy sold to the grid. These three energy terms represent the total amount of  
 381 useful energy that the system produces per year. The levelized cost of energy is the average  
 382 cost for each kWh of useful electrical energy produced by the system. It is worth noting that  
 383 all comparisons that HOMER establishes between different configurations are based on the  
 384 net present cost, since - in the literature - the definition of the levelised cost of energy is more  
 385 disputed than the definition of the net present value (*Lambert et al., 2006*).

#### 386 4. System modelling

387 As previously introduced in section 1, it is assumed the renewable energy technologies are in  
388 parallel to the main electricity grid (see Figure 3), since the electrification rate in urban areas  
389 of Sub-Saharan Africa is over 60% with several electrification projects currently under  
390 development (*Zeyringer et al., 2015*). Figure 3 summarizes the alternative renewable systems  
391 considered in this study, which included a Combined Heat and Power system fuelled by  
392 biogas produced from the wastewater sludge, photovoltaic units, and wind turbines. The  
393 electricity load is AC-coupled to the electricity grid, as well as the wind turbine and  
394 combined heat and power units, while the photovoltaic units and batteries are DC-coupled.  
395 An internal combustion engine, ICE, in cogeneration mode was assumed to be able to  
396 produce energy using the biogas coming from the anaerobic digester. This is one of the most  
397 commonly applied configurations worldwide, since the heat recovered by the combined heat  
398 and power unit is used to satisfy the heat demands of the anaerobic process (*Silvestre et al.,*  
399 *2015*).

400 The sizes of the combined heat and power unit and photovoltaic system were varied  
401 in steps of 5 kW<sub>el</sub> from 0 kW<sub>el</sub> up to the peak load. A step size of 10 kW<sub>el</sub> was chosen for the  
402 wind turbine system. Table 2 presents the main techno-economic data for the renewable  
403 technologies assessed; most of this information was derived from default data available in the  
404 HOMER library. Clearly, the technology lifetime varies for each renewable system, ranging  
405 from 48,000 hours for the internal combustion engine (almost 6 years considering 8600  
406 operating hours) to 25 years for a photovoltaic system. For the internal combustion engine  
407 modelled in HOMER, the loss in electrical efficiency when working at partial loads has also  
408 been considered; at the minimum load ratio of 40%, electrical efficiency drops from 38% to  
409 35%. The use of photovoltaic units requires a DC to AC converter (Fig. 3). A default

410 converter has been considered. The capital cost has been assumed to be \$300, with a lifetime  
411 of 15 years, inverter efficiency of 90% and rectifier efficiency of 85%.

#### 412 *4.1 Resource assessment*

413 The natural resources used for energy production need to be defined by the modeller. The  
414 renewable energy resources considered in the present analysis are wind energy, solar energy  
415 and biogas. HOMER provided data on solar insolation and wind speed, which was obtained  
416 via the internet from international meteorological centres. The annual average wind speed for  
417 the reference location is 3.7 m/s at an anemometer height of 50 m. Figure 4 shows the  
418 monthly average wind speed for the specific location. The variation in wind speed, which is  
419 given by the autocorrelation factor, is 0.85, with 15 hours of peak wind speed and a diurnal  
420 pattern strength (i.e. the magnitude of the average daily pattern of wind speed) of 0.25.

421 For photovoltaic production, a typical meteorological year is considered for the  
422 specified location. The annual solar radiation at the latitude of 8° 58.8'N and longitude of 38  
423 °45.5'E is 5.81 kWh/m<sup>2</sup>/day with an average sky clearness of 0.68 (Fig. 5). As expected, solar  
424 radiation is available throughout the year, with a high potential for electricity production  
425 from solar energy of 2,306 kWh for each kW<sub>el</sub> of photovoltaic unit installed.

426 Biogas produced from the organic content of the wastewater passing through the  
427 anaerobic digestion system has also been considered. The quantity of biogas produced has  
428 been defined as the fraction of the chemical oxygen demand removed during wastewater  
429 treatment (Table 1). Figure 6 shows the biogas monthly resource input, which has been  
430 defined according to Eq. 4.

431

432 *Biogas availability*

433 
$$= WW \text{ available} \times \frac{COD}{WW \text{ treated}} \times COD \text{ removal efficiency}$$

434 
$$\times \frac{\text{biogas produced}}{COD \text{ removed}}$$

435 (4)

436 A chemical oxygen demand removal efficiency of 70% is assumed (*Khiewwiji et al., 2015*).  
437 These data were used by HOMER to generate an annual series of biogas hourly available for  
438 electricity production.

439 When the electricity needs of the wastewater treatment facility are not satisfied by  
440 renewable energy sources, the Ethiopian energy mix has been considered, whereby - on  
441 average - 88% of electricity comes from hydropower, 11% from diesel generators and 1%  
442 from geothermal energy (*Energypedia, 2016*). We have not taken any thermal needs into  
443 consideration, but have assumed the thermal energy produced by the biogas unit is entirely  
444 used internally for the anaerobic digestion process. In emergencies, electricity cannot be  
445 provided by the central grid. It is assumed that a diesel engine will be used in such situations.  
446 Table 3 summarizes the main characteristics of the energy resources considered in this  
447 analysis.

#### 448 *4.2 Scenarios analysed*

449 Three different scenarios (Table 4) have been analysed: i) baseline, ii) emergency, and iii)  
450 “selling electricity back” scenario. The baseline scenario takes three different electricity  
451 tariffs into account. The current electricity tariff in Ethiopia is 0.04 \$/kWh, which is one of  
452 the lowest and most subsidised rates in Sub-Saharan Africa (*Bekele and Tadesse, 2012*).  
453 Since the current cost of electricity is not representative of the true cost of electricity and is  
454 underestimated by 50% (*Foster and Morella, 2011*), a tariff of 0.08 \$/kWh has been  
455 considered in the baseline scenario. Finally, a tariff of 0.16 \$/kWh is also used in the baseline  
456 scenario, which represents the long-term marginal cost of power when the costs of building  
457 and operating an effective full coverage transmission and distribution network in Ethiopia is  
458 considered (*Foster and Morella, 2011*). For the baseline scenario, it is assumed that excess

459 electricity cannot be sold back to the national grid, since at a low voltage this would require  
460 the systems to be supplemented with additional safety provisions.

461         Considering there are approximately 40 days (*Foster and Morella, 2011*) of power  
462 outage in Ethiopia per year and wastewater treatment cannot be stopped, an emergency  
463 scenario has been analysed, in which electricity is produced for 40 days per year by a diesel  
464 engine at a tariff of 0.9 \$/kWh (*Bekele and Tadesse, 2012*). Finally, a selling tariff of 200  
465 US\$/MWh for the electricity sold back to the grid, has been considered (“selling electricity  
466 back” scenario). It is equal to the feed in tariff currently provided by the government of  
467 Kenya for supporting the photovoltaic production (*Kebede, 2015*).

468

## 469 **5. Results and Discussion**

470 Table 5 presents the technical results of the simulations developed by HOMER in three  
471 scenarios for a wastewater treatment facility with a conventional activated sludge system  
472 situated in Sub-Saharan Africa. The table presents the size, number of operating hours and  
473 electricity produced by the various renewable technologies considered in the micro-  
474 generation system, as follows: i) an internal combustion engine fuelled by biogas produced in  
475 the wastewater treatment plant; ii) photovoltaic units; and iii) a wind turbine. The energy  
476 capacity of lead acid batteries is also shown. The results are ordered from minimum to  
477 maximum net present cost, the main criterion employed in the HOMER analysis. Table 6  
478 summarises the main economic parameters for the solutions identified, including initial  
479 investment, cost of energy and net present cost. Table 6 also shows the renewable fraction  
480 from local resources, the amount of electricity purchased, the amount of biogas used by the  
481 internal combustion engine and the surplus electricity coming from intermittent renewable  
482 sources (i.e. wind and solar energy). It is worth noting the renewable fraction only considers

483 local renewable energy sources. In fact, as mentioned above, 89% of the electricity supplied  
484 by the national grid in Ethiopia is generated from renewable sources.

#### 485 *5.1 Solutions for a wastewater treatment facility with a conventional activated sludge system*

486 The HOMER analysis indicates that, at the current Ethiopian electricity tariff of 0.04  
487 \$/kWh, investment in renewable technologies is not economically viable. At this subsidized  
488 tariff, purchasing electricity from the grid is the best option from an economic point of view.  
489 For this solution (solution A), the net present cost shown in Table 6 is determined from the  
490 Operating and Maintenance, O&M, cost of the grid. The first solution with a renewable  
491 energy system (solution B) proposed by HOMER is a 5 kW<sub>el</sub> internal combustion engine  
492 fuelled by biogas, which would slightly increase the levelised cost of energy to 0.041 \$/kWh,  
493 and cover 11% of the electrical load. The investment required for solution B is \$7,500, and  
494 there is no excess electricity that is not used by the wastewater treatment facility.

495 These predictions for a wastewater treatment facility located in a specific location of  
496 Ethiopia are in line with the literature. *Bekele and Tadesse (2012)* argued that the use of  
497 renewable technologies for electricity production in an Ethiopian district is not profitable at  
498 the current electricity tariff of 0.04 \$/kWh. Therefore, a higher tariff that takes into account  
499 the true cost of electricity is necessary to make the use of local renewable energy sources  
500 economically desirable. At an electricity tariff of 0.08 \$/kWh, several possible configurations  
501 of renewable energy technologies are characterised by a lower net present cost and lower  
502 levelised cost of energy than conventional energy generation. The minimum net present cost  
503 is achieved for solution A, a 15 kW<sub>el</sub> internal combustion engine fuelled by biogas. The size  
504 of the internal combustion engine is limited by the maximum amount of biogas available  
505 from wastewater treatment. The internal combustion engine works 8,760 hours per year,  
506 highlighting the convenience of using biogas for electricity generation (*Hao et al., 2015*). In

507 this solution, approximately one-third of the electricity demand can be supplied by local  
508 renewable energy sources.

509 A slightly higher cost of energy, 0.070 \$/kWh, is predicted for a higher fraction from  
510 local renewable sources (35%). HOMER identifies solution B, a combination of a 15kW<sub>el</sub>  
511 biogas system and a 5kW<sub>el</sub> photovoltaic system, which is able to produce 11,531 kWh per  
512 year, operating for 4,469 hours.

513 A further suggested system, solution C, with a cost of energy of 0.074 \$/kWh, is the  
514 combination of a 15kW<sub>el</sub> internal combustion engine fuelled by biogas with a 10 kW<sub>el</sub> wind  
515 turbine. In this solution, the amount of electricity produced from local renewable sources is  
516 slightly lower than for solution B (33.3%), since the 10 kW<sub>el</sub> wind turbine produces less  
517 energy (2,656 kWh per year) than a 5 kW<sub>el</sub> photovoltaic unit, due to the characteristically  
518 high level of solar radiation in the area. The last solution identified by HOMER, solution D,  
519 suggests the integration of a 15 kW<sub>el</sub> biogas system with a 5 kW<sub>el</sub> photovoltaic unit and  
520 10 kW<sub>el</sub> wind turbine. The investment cost and net present cost increase; however, this  
521 combination of three micro-generation units provides a higher renewable fraction of 36%.  
522 Although solution D works for the same number of operating hours thorough the year as  
523 solution A, the 15kW<sub>el</sub> internal combustion engine produces slightly less electricity in  
524 solution D. This indicates the internal combustion engine is modulated to allow all of the  
525 energy produced by the intermittent renewable technologies (photovoltaic system and wind  
526 turbine) to be used by the wastewater treatment facility. In all of the cases proposed by  
527 HOMER at the 0.08 \$/kWh tariff, there is no excess of electricity produced by the  
528 intermittent renewable sources.

529 When the electricity tariff increases, the renewable technologies selected by HOMER  
530 change, highlighting how the results of this analysis are strongly affected by the cost of  
531 electricity from the grid. The optimal solution selected for tariff of 0.16 \$/kWh is a 15kW<sub>el</sub>

532 internal combustion engine fuelled by biogas combined with a 50 kW<sub>el</sub> photovoltaic system  
533 (solution A). The size of the internal combustion engine does not change with the tariff, since  
534 its maximum size is limited by the amount of biogas available from the wastewater treatment  
535 facility, as previously mentioned. A larger photovoltaic system allows a 55% renewable  
536 fraction. In contrast to the previous solutions, a small amount of electricity, 3,880 kWh  
537 (around 1% of the electricity needs) is produced in excess by solution A and not used by the  
538 wastewater treatment facility. Comparing the number of operating hours for the internal  
539 combustion engine system with and without a photovoltaic unit (solutions A vs. solutions B  
540 and C), it is clear that the operating hours of the internal combustion engine reduce when it is  
541 coupled to a photovoltaic system. As shown in Fig. 7, modulating the electrical output of the  
542 internal combustion engine helps to reduce the excess electricity produced from intermittent  
543 renewable sources; when production by the photovoltaic system occurs at the highest rate,  
544 between 8:00 a.m. to 4:00 p.m., production by the internal combustion engine is drastically  
545 reduced to lessen the amount of excess electricity produced from intermittent renewable  
546 sources.

547         However, a battery is required to reduce the electricity in excess to zero, as shown in  
548 solution G, in which a 50 kW<sub>el</sub> photovoltaic system is combined with a 15 kW<sub>el</sub> internal  
549 combustion engine and a storage unit with a storage capacity of 350 kWh. While batteries  
550 remain expensive (*Wang et al., 2016*), research in this field is active and the study of  
551 rechargeable batteries based on low-cost materials is promising. For this specific location, the  
552 maximum size of the wind turbine selected by the model is 10 kW<sub>el</sub>; the size of the wind  
553 turbine is limited by the average wind speed and the trade-off between investment and the  
554 savings in operating cost.

555         In the emergency scenario, with 40 days covered by electricity produced by a diesel  
556 engine at a cost of 0.9 \$/kWh for diesel, the investment in renewable technologies is always

557 economically viable and desirable. For the emergency scenario, the average electricity tariff  
558 is 0.134 \$/kW, based on 40 days at 0.9 \$/kWh for diesel and the remainder of the year at  
559 0.04 \$/kWh. The solution characterised by the lowest net present cost, solution A in Table 6,  
560 is the coupling of a 35 kW<sub>el</sub> photovoltaic system and 15 kW<sub>el</sub> internal combustion engine  
561 fuelled by biomass. The renewable coverage from local resources would be 48%, with a  
562 small excess of electricity of 591.5 kWh/year, which represents 0.16% of electricity needs.  
563 Table 6 also shows the other possible solutions with a levelised cost of energy lower than the  
564 true cost of electricity. The initial investment ranges from 100,000 to 160,000 US dollars,  
565 with a coverage by renewables ranging from 26% to 48%. The use of high rate photovoltaic  
566 systems of 55 kW<sub>el</sub> and 50 kW<sub>el</sub> increases the amount of electricity in excess (about 4% of  
567 the electricity demand), requiring the use of batteries or providing an opportunity to sell  
568 excess electricity back to the grid.

569 In the “selling electricity back” scenario, a selling tariff of 200 \$/MWh has been  
570 considered. As mentioned above, this value is equal to the feed-in tariff introduced by Kenya  
571 in order to support the introduction of photovoltaic systems. At the current Ethiopian  
572 electricity tariff of 0.04 \$/kWh, investment in renewable technologies is still more viable than  
573 buying electricity from the grid. However, as shown by solution C of the feed-in tariff  
574 scenario (Tables 5 and 6), coupling a 15kW<sub>el</sub> biogas system with a 120 kW<sub>el</sub> photovoltaic unit  
575 provides a lower levelised cost of energy than the electricity tariff, thanks to the revenues  
576 generated by selling excess electricity back to the grid. For this solution, the renewable  
577 fraction reaches 74%, with a small amount of excess electricity of 946 kWh, which is 0.2% of  
578 total electrical demand.

579 *5.2 Solutions for a wastewater treatment facility containing a membrane bioreactor for water*  
580 *reuse*

581 Tables 7 and 8 show the analyses for the case of a wastewater treatment facility with a  
582 membrane bioreactor to enable the reuse of reclaimed wastewater for irrigation. In this case,  
583 the electricity demand is more than seven times higher than a wastewater treatment facility  
584 based on a conventional activated sludge system. In the baseline scenario at the tariffs of 0.04  
585 \$/kWh and 0.08 \$/kWh, there is no change in the size of the renewable technologies between  
586 the facilities with a membrane bioreactor and conventional activated sludge technology. As a  
587 consequence, the coverage of the electrical loads from renewable sources reduces to 5% for  
588 the wastewater treatment facility with a membrane bioreactor. In this case, the higher  
589 electricity tariff of 0.016 \$/kWh tariff justifies the introduction of a 120kW<sub>el</sub> photovoltaic  
590 system, which combined with a 15 kW<sub>el</sub> internal combustion engine and 10 kW<sub>el</sub> wind  
591 turbine covers 13% of the electricity needs of the wastewater treatment facility. For solution  
592 D, the batteries selected are not able to reduce the electricity in excess to zero.

593 As shown in Table 7, the optimal size of photovoltaic system selected by HOMER for  
594 the wastewater treatment facility with a membrane bioreactor increases compared to the case  
595 of conventional activated sludge technology. The size of the other renewable technology  
596 units cannot change, due to limitations on resource availability, although increasing the size  
597 of renewable technologies would be convenient from an economic point of view.

598 HOMER did not select any high rate photovoltaic system for the ‘selling electricity  
599 back” scenario for the wastewater treatment facility with a membrane bioreactor, as in the  
600 case of the conventional activated sludge facility. As shown in Table 7, the sizes of the  
601 renewable technologies selected by HOMER for the wastewater treatment facility with a  
602 membrane bioreactor are the same as for the 0.04 \$/kWh baseline case. Even a 120 kW<sub>el</sub>  
603 photovoltaic system would not generate any income, since all of the electricity would be used  
604 by the wastewater treatment facility with a membrane bioreactor as the total electrical  
605 demand is more than seven times higher than for conventional activated sludge technology.

606 **6. Post-HOMER analysis of the proposed solutions in the context of socio-political and**  
607 **security**

608 This section provides a post-HOMER analysis to discuss the merits of the identified technical  
609 solutions against the socio-political and security background of the region. We analyse how  
610 the technical approaches proposed in this work can contribute to simultaneously address  
611 several socio-political pressures and reduce both domestic and cross-border conflicts.

612 As explained in the introductory chapter, the rapidly growing population in Sub-  
613 Saharan Africa is experiencing increasing hardships due to climate change, a lack of water  
614 and electricity, and deteriorating environmental quality. All of these factors contribute – in  
615 one way or another – to both human insecurity and transboundary tensions or even conflicts.  
616 In the context of sustainable development, it has become helpful to distinguish the concept of  
617 human security from the more conventional idea of national (state) security (*Hove et al.,*  
618 *2013; UNDP, 1994*). Whereas state security addresses the defence of a country within its  
619 international borders, the concept of human security focuses on the security concerns of  
620 ordinary people in their daily lives, encompassing protection from the threat of disease,  
621 hunger, lack of water, unemployment, crime, social conflict/exclusion, political repression  
622 and environmental hazards. With respect to water issues, both state and human insecurity  
623 play a key role in Sub-Saharan Africa, where some 30% of the population live in semi-arid  
624 areas (*Tiffen, 2003*). Malnutrition is severe, food imports are increasing steadily, and food aid  
625 remains a common relief measure (*Reij and Smaling, 2008*). Rural-to-urban migration is the  
626 single most important cause of the rapid growth of the urban population of the region; over  
627 70% live in urban slum dwellings that lack sanitation and other basic services (*Hove et al.,*  
628 *2013*).

629 Much of the highest population growth is occurring in places that are already  
630 vulnerable to water scarcity, with climate change aggravating the scarcity of water, cropland

631 and pasture. Resource scarcity will likely increase its weight as a motivation for violent  
632 conflict over time (*Matthew, 2012*). Policies related to agriculture, food subsidies and  
633 exchange rates have tended to keep food prices low for urban consumers, but at the expense  
634 of farmers (*Hove et al., 2013; IBRD, 1989*). Largely due to these policies, the level of  
635 urbanization in Sub-Saharan Africa has increased dramatically and is currently almost 40%.  
636 The UN Population Fund projected the urban population of Africa will double between 2000  
637 and 2030 (*UNFPA, 2007*). According to some estimates, the situation in Sub-Saharan Africa  
638 is even more worrying: the urban population of the region doubled between 2000 and 2015,  
639 and over half of this population cooks on open fires or inefficient stoves using fuel wood,  
640 charcoal or dung, resulting in high levels of indoor pollution and severe health impacts.  
641 Moreover, in 2015, 66% of the urban population in Sub-Saharan Africa did not have water  
642 piped onto their premises, representing a small increase from only 57% in 1990  
643 (*Satterthwaite, 2015*).

644 As pointed out by many researchers, the electrical power infrastructure in Sub-  
645 Saharan Africa is significantly underdeveloped, leading to deficits in energy access, installed  
646 capacity, and per capita consumption (*Castellano, 2015*). Countries with electrification rates  
647 of less than 80% exhibit reduced GDP per capita. The level of electricity-access in Sub-  
648 Saharan Africa is the poorest in the world, with 48% of the population lacking access.  
649 According to *Castellano (2015)*, it takes an average of 25 years to progress from an  
650 electrification rate of 20% to 80%.

651 Conflicts may be domestic – restricted to one country – but, as is the case for water  
652 issues, a variety of transboundary conflicts can occur; such conflicts concern both water  
653 quantity and water quality, often in connection with food production and energy supply  
654 issues. How can the integration of renewable energy sources with wastewater treatment

655 facilities, as proposed in the earlier sections of this work, contribute to mitigate the security  
656 risks related to the water-energy nexus in Sub-Saharan Africa?

657         Firstly, the HOMER analysis indicates renewable energy sources can cover up to 55%  
658 of the electricity demand for standard wastewater treatment facilities in this region. This  
659 approach could help to overcome one of the major barriers to the implementation of  
660 wastewater treatment facilities, a lack of energy. Protecting water bodies from direct  
661 wastewater discharge and avoiding a high incidence of water-borne diseases will help to  
662 maintain social cohesion and stability, especially under conditions of prevailing poverty,  
663 extremely rapid population growth, and migration from rural to urban and semi-urban areas.  
664 Therefore, introduction of the proposed waste-water technologies in urban and semi-urban  
665 areas can also be justified from a security perspective.

666         Secondly, lack of electricity is more than just an inconvenience – it can be life-  
667 threatening. Large numbers of schools and health centres operate without electricity. Without  
668 proper health and education, the chances of the population escaping poverty remain slim to  
669 none. However, an electricity infrastructure can only be deployed and operated in a  
670 financially-sustainable electricity sector that can recover its costs, make investments, provide  
671 electricity reliably and meet social and environmental obligations. The HOMER analysis  
672 demonstrates renewable energy sources are techno-economically viable solutions, even when  
673 considering the true cost of electricity or typical days of power outage per year. Furthermore,  
674 the proposed integration of renewable energy sources in wastewater treatment facilities may  
675 improve the resilience of the energy system, providing a solution for the days of power  
676 outage at a levelised cost of energy lower than the electricity tariff.

677         Thirdly, a positive impact on human security arises from the growth in jobs. Any  
678 technology, whether built by foreign or local contractors, plays a significant role in the  
679 capacity-building of local actors. Both wastewater and renewable energy technologies

680 comprise civil, hydraulic, mechanical and electrical (electromechanical) engineering  
681 structures. Therefore, the stakeholders, experts, contractors, consultants, labourers, small  
682 business and microenterprises will have the opportunity to build capacity either during the  
683 manufacturing and installation phase or during operating and maintenance. Renewable  
684 energy generation can increase local employment; typical employment factors for solar  
685 photovoltaic systems are 25 people/MW for manufacture and installation, and 2.5 jobs/MW<sub>el</sub>  
686 for operation and maintenance (*Brandoni et al, 2016*).

687         Fourthly, the proposed integration is capable of mitigating certain cross-boundary  
688 impacts, both in terms of water quantity and quality. Although the proposed techno-  
689 economically viable solutions can only cover 13% of the total electrical demand in the case  
690 of water reuse, the integration of renewable technologies into wastewater treatment facilities  
691 can attract new investors, providing access to both adaptation and mitigation funds (*Climate*  
692 *Investment Fund, 2014*). Water reuse offers an alternative for the development of small-scale  
693 irrigation schemes, without the construction of storage systems that could be a further source  
694 of potential conflict. Considering an irrigation need of 4,200 m<sup>3</sup> per ha (*Maton et al., 2010*)  
695 and a cultivated area per person of 0.17 ha (*Home and Sale, 2011*), a wastewater treatment  
696 facility serving 10,000 people produces enough water to irrigate a cultivated area of  
697 approximately 190 ha, which could feed about 1,100 people for 41 days. This is a significant  
698 contribution that could contribute to locally relieve the food insecurity of the impoverished  
699 and dissatisfied urban and semi-urban population. *Rockström et. al.* (2010) argued the local  
700 catchment scale offers the best opportunities for water investments to build resilience in  
701 small-scale agricultural systems and address trade-offs between the use of water for food and  
702 other ecosystem functions and services. The Abay (Blue Nile) drainage basin covers 180,000  
703 km<sup>2</sup> (20% of Ethiopia's land area) and is home to around 20 million people. The water flow  
704 in the Blue Nile averages 48 billion m<sup>3</sup> at the Sudanese border (*Johnston and McCartney,*

705 2010). The potential water quantity savings from the Blue Nile can be calculated by assuming  
706 a wastewater treatment facility servicing a population of 10.000, treating 0.8 million m<sup>3</sup>/year  
707 and yielding the same amount of irrigation water to avoid diverting the same amount of water  
708 from other sources. If all inhabitants of the Blue Nile drainage basin could make use of such  
709 facilities, 12% of total irrigation needs would be satisfied, equalling an upper limit of 1.6  
710 billion m<sup>3</sup>/year to be saved, or 3.3% of the total flow of the Blue Nile at the Sudanese border.  
711 While this volume is not dramatic, it carries moral significance as a confidence building  
712 measure in the context of transboundary negotiations between upstream and downstream  
713 countries. Moreover, the provision of wastewater treatment facilities area-wide would  
714 presumably have favourable impacts on health and environment, not only locally but also  
715 cross-border downstream.

716         Precise assessment of the positive effects of deploying the proposed integration of  
717 renewable energy technologies with wastewater treatment facilities in Sub-Saharan Africa  
718 depends on a number of external unknowns. Reliable basic data are not available on the  
719 processes and consequences of ongoing urbanization; on the extent of - and obstacles to -  
720 deployment of treated water for irrigation; on environmental and health impacts, both locally  
721 and downstream due to the lack of solid waste management and wastewater treatment  
722 facilities; and the fact a financially sustainable electricity sector is still lacking, preventing  
723 steady deployment of renewable energy technologies. To address security issues, the sharing  
724 of information at all levels is of utmost importance. The obligation to share data and  
725 information on a regular basis is a principle of international customary water law, which is  
726 definitively expressed in water-related conventions. Studies on cooperation in African river  
727 and lake basins show formal information-sharing agreements are often preceded by projects  
728 designed to improve the information basis (*Wirkus and Böge, 2006*). The ability to access  
729 accurate information increases the likelihood of agreements that are technically and

730 economically feasible, deliver their promised benefits and produce no significant negative  
731 side-effects (or even unexpected positive outcomes). Joint research involving several  
732 stakeholders is likely to result in fewer technical controversies than research by individual  
733 stakeholders.

734

## 735 **7. CONCLUSIONS**

736 This work investigated the benefits of integrating renewable energy technologies with a  
737 wastewater treatment facility located in arid regions of water-stressed urban areas. An urban  
738 area of Sub-Saharan Africa has been selected to accurately consider the electrical loads of a  
739 wastewater treatment facility based on a conventional activated sludge system and a  
740 wastewater treatment facility based on a membrane bioreactor so the treated water can be  
741 reused for irrigation.

742         The HOMER analysis showed the introduction of technology that harvests local  
743 renewable energy sources to satisfy some of the electrical load of a wastewater treatment  
744 facility is cost-effective if the true cost of energy is considered or if the costs of covering the  
745 days of power outage is taken into account. The integration of renewable technologies is  
746 predicted to provide good coverage of the electrical load required by a wastewater facility  
747 based on a conventional activated sludge system, achieving a 33% renewable fraction at an  
748 electricity tariff of 0.08 \$/kWh (true cost of electricity considering the current transmission  
749 and distribution network), 55% at an electricity tariff of 0.016 \$/kWh tariff (true cost of  
750 building and operating an effective full coverage transmission and distribution network in  
751 Ethiopia), 48% in the emergency scenario, and up to 74% if a selling back electricity price of  
752 200 \$/MWh is considered.

753         Currently, less than 30% of wastewater is treated in Sub-Saharan Africa. This work  
754 highlights the fact that integration of renewable energy technologies would help to overcome

755 one of the main barriers to the widespread deployment of wastewater treatment facilities,  
756 which is a lack of electricity. The emergency scenario shows the predicted solution could also  
757 help to improve the reliability of the electrical grid at a levelised cost of energy lower than  
758 the cost of using diesel engines to satisfy the electrical demands of the facility during power  
759 outages. Furthermore, in all of the solutions identified, even those with a high renewable  
760 fraction, the electricity in excess is never greater than 4% of the electrical demand. Therefore,  
761 the developments proposed in this work would have minimal impact on the national  
762 electricity grid.

763 In the case of water reuse, the cost-effective solutions selected by HOMER cover a  
764 smaller percentage of the electricity needs of the wastewater treatment facility with a  
765 membrane bioreactor (up to 13%). This is mainly associated with the high electrical demand  
766 of treating wastewater for reuse, the constraints affecting some local renewable energy  
767 sources (i.e. biogas) and the high investment cost of renewable technologies. However, as  
768 explored in section 6 of this paper, adoption of the proposed technologies may exert several  
769 positive impacts on communities, such as the mitigation of security risks at both the domestic  
770 and cross-border levels.

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991 Microbial Bioreactor system (Economic results, electricity purchased, biogas consumption,  
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1000	Table 1. Main parameters of the influent wastewater ( <i>Henze, 2002; Khiewwijit et al., 2015</i> )	
	COD [mg/L]	500
	SS [kg/(person*year)]	20
	CH <sub>4</sub> [g/gCOD <sub>removed</sub> ]	0.23

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**Table 2. Main techno-economic data for the renewable technologies assessed**

<b>CHP unit – Internal Combustion Engine</b>	
Electrical efficiency [%]	38
Thermal efficiency [%]	50
Lifetime (hours)	48,000
Minimum load [%]	40
Capital cost (\$/kWh)	1,500
O&M costs (\$/kWh)	0.021
<b>PV systems</b>	
Efficiency [%]	17
Capital cost (\$/kW)	2,500
Lifetime	25
<b>Wind system (Generic 10kW)</b>	
Power output (kW)	10
Capital cost (\$/unit)	20,000
Lifetime	20
<b>Batteries (Generic 1kWh Lead Acid)</b>	
Nominal voltage [V]	12
Nominal capacity [Ah]	83.3
Cost (\$/kWh)	300
Lifetime (kWh)	800

1004

1005

1006 Table 3. Main characteristics of the energy resources considered in this analysis

<b><i>Resources</i></b>	<b><i>Description parameters</i></b>
Biogas	Low heating value of 5.5 MJ/kg
Solar energy	Solar radiation of 5.81 kWh/m <sup>2</sup> /day, clearness factor of 0.60
Wind	Average wind speed of 3.7 m/sec
Local energy mix for electricity supply	88% hydropower, 11% diesel, 1% geothermal energy
Diesel for emergency scenario	0.9 \$/kWh

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1008

1009 Table 4. Scenarios analysed

	<i>Electricity prices</i>	<i>Electrical demand [MWh/year]</i>		<i>Water treated [m<sup>3</sup>/year]</i>
		<i>Conventional Activated Sludge</i>	<i>Membrane bioreactor</i>	
<i>Baseline Scenario</i>	0.04 \$/kWh 0.08 \$/kWh 0.16 \$/kWh			
<i>Emergency Scenario</i>	0.04 \$/kWh 41 days @ 0.9\$/kWh	402	2,945	793,356
<i>“Sell electricity back” scenario</i>	0.04 \$/kWh Selling tariff of 0.2 \$/kWh			

1010

1011

1012 Table 5. Simulation results in three scenarios for a wastewater treatment facility with a  
 1013 conventional activated sludge system (Nominal power, working hours and electricity  
 1014 production of micro-generation technologies)

<b>Baseline scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
0.04\$/kWh										
A										
B		5			8,760			43,800		
0.08\$/kWh										
A		15			8,760			131,337		
B	5	15		4,469	8,760		11,531	131,316		
C		15	10		8,760	4,698		131,271	2,656	
D	5	15	10	4,469	8,760	4,698	11,531	131,240	2,656	
0.016 \$/kWh										
A	50	15		4,469	8,234		115,306	119,763		
B	45	15	10	4,469	8,378	4,698	103,775	122,093	2,656	
C		15			8,760			131,337		
D		15	10		8,760	4,698		131,217	2,656	
E	70			4,469			161,428			
F	65		10	4,469		4,698			2,656	
G	50	15		4,469	8,234		115,306	119,763		350
<b>Emergency scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
A	35	15		4469	8,195		80,714	122,364		
B	35	15	10	4469	8,156	4689	80,714	121,273	2,656	
C		15	10		8,695	4689		130,382	2,656	
D	55			4469			126,837			
E	50		10	4469		4689	115,306		2,656	
<b>“Selling electricity back” scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
A										
B		5			8760			43,800		
C	120	15		4469	8760		276,735	131,400		

1015  
1016

1017 Table 6. Simulation results in three scenarios for a wastewater treatment facility with a  
 1018 conventional activated sludge system (Economic results, electricity purchased, biogas  
 1019 consumption, renewable fraction, excess electricity)

<b>Baseline scenario</b>							
<i>Solutions</i>	<i>Initial investment</i> [\$]	<i>COE</i> [\$]	<i>NPC</i> [\$]	<i>Electricity purchased</i> [kWh]	<i>Biogas</i> [kg/year]	<i>Renewable fraction</i> [%]	<i>Excess electricity</i> [kWh]
<b>0.04\$/kWh</b>							
A	/	0.040	208,185	402,601	/	/	/
B	7,500	0.041	212,276	358,801	31	11.0	/
<b>0.08\$/kWh</b>							
A	22,500	0.069	360,762	271,264	94	32.6	/
B	36,500	0.070	365,214	260,907	94	35.2	/
C	42,500	0.074	386,253	268,673	94	33.3	/
D	56,500	0.075	390,717	258,327	94	35.8	/
<b>0.016\$/kWh</b>							
A	159,500	0.116	601,521	182,555	86	55.0	3,880
B	165,500	0.120	625,232	187,211	88	53.5	3,063
C	22,500	0.123	641,303	271,264	94	32.6	/
D	42,500	0.128	664,115	268,273	94	33.3	/
E	191,500	0.147	766,408	270,825	/	32.7	15,011
F	197,500	0.152	789,978	279,931	/	31.5	12,105
G	264,500	0.160	831,952	182,555	86	54.7	/
<b>Emergency scenario</b>							
<i>Solutions</i>	<i>Initial investment</i> [\$]	<i>COE</i> [\$]	<i>NPC</i> [\$]	<i>Electricity purchased</i> [kWh]	<i>Biogas</i> [kg/year]	<i>Renewable fraction</i>	<i>Excess electricity</i> [kWh]
A	119,000	0.094	487,289	208,126	88	48	591.5
B	139,000	0.098	509,417	206,168	87	49	653.8
C	42,500	0.102	530,340	269,563	94	33	0
D	151,00	0.119	620,066	293,129		27	5,200
E	158,500	0.123	642,623	299,053		26	3,204
<b>“Selling electricity back” scenario</b>							
Scenario	Initial investment	COE	NPC	Electricity purchased	Fuel kg/year	Renewable coverage	Excess electricity
A	0	0.040	208,185			0	/
B	7,500	0.041	212,276	358,801	31	11	/
C	352,500	0.032	215,028	135,064	94	74	946,4

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Table 7. Simulation results in three scenarios for a wastewater treatment facility with a Microbial Bioreactor system (Nominal power, working hours and electricity production of micro-generation technologies)

<b>Baseline scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries Capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
0.04\$/kWh										
A										
B		5			8,760			43,800		
C	5			4,469			11,531			
0.08\$/kWh										
A		15			8,760			131,337		
B	5	15		4,469	8,760		11,531	131,316		
C		15	10		8,760	4,698		131,271	2,656	
D	5	15	10	4,469	8,760	4,698	11,531	131,240	2,656	
0.016 \$/kWh										
A	120	15		4,469	8,760		276,735	131,400		
B	120	15	10	4,469	8,760	4,698	276,735	131,400	2,656	
C		15			8,760			131,400		
D		15	10		8,760	4,698		131,400	2,656	
E	120			4,469			276,735			
F	120		10	4,469		4,698			2,656	
G	120	15		4,469	8,760		276,735	131,400		350
<b>Emergency scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries Capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
A	120	15		4469	8,760		276,735	131,400		
B	120	15	10	4469	8,760	4689	276,735	131,400	2,656	
C		15			8,760			131,400		
D	120	15		4469	8,760		276,735	131,400		350
E	120	15	10	4469	8,760	4689	276,735	131,400	2,656	
<b>“Selling electricity back” scenario</b>										
<i>Solutions</i>	<i>Nominal Power [kW]</i>			<i>Working hours</i>			<i>Production (kWh/year)</i>			<i>Batteries Capacity [Ah]</i>
	PV	ICE	Wind	PV	ICE	Wind	PV	ICE	Wind	
A										
B		5			8,760			43,800		
C	5	/	/	4,469			11,531			

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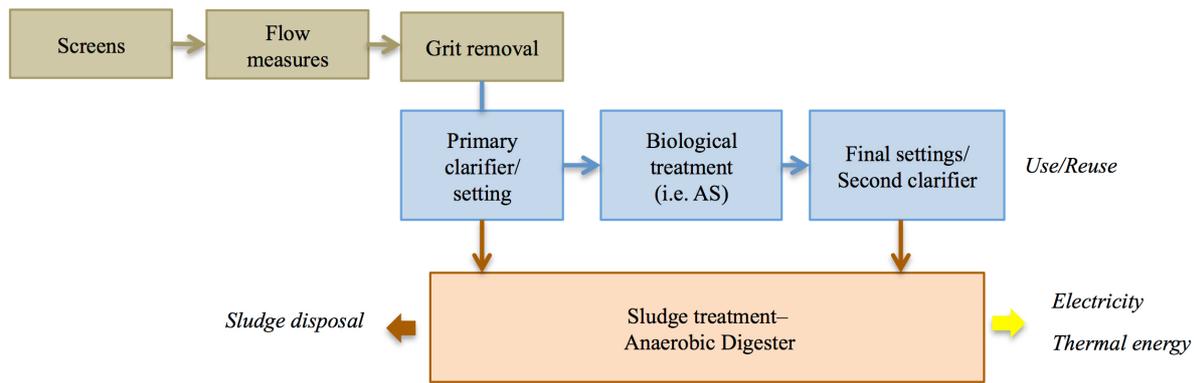
1027 Table 8. Simulation results in three scenarios for a wastewater treatment facility with a  
 1028 Microbial Bioreactor system (Economic results, electricity purchased, biogas consumption,  
 1029 renewable fraction, excess electricity)

<b>Baseline scenario</b>							
<i>Solutions</i>	<i>Initial investment</i> [\$]	<i>COE</i> [\$]	<i>NPC</i> [k\$]	<i>Electricity purchased</i> [MWh]	<i>Biogas</i> [kg/year]	<i>Renewable fraction</i> [%]	<i>Excess electricity</i> [kWh]
0.04\$/kWh							
A	0	0.040	1,523	2,945			
B	7,500	0.040	1,527	2,902	31	1	
C	14,000	0.040	1,533	2,935		0.4	
0.08\$/kWh							
A	22,500	0.079	2,991	2,815	94	4	
B	36,500	0.079	2,995	2,804	94	5	
C	42,500	0.079	3,016	2,811	94	5	
D	56,500	0.079	3,020	2,801	94	5	
0.016\$/kWh							
A	352,500	0.151	5,744	2,566	94	13	946
B	372,500	0.151	5,766	2,563	94	13	946
C	22,500	0.155	5,901	2,814	94	4	
D	42,500	0.156	5,924	2,811	94	5	
E	330,500	0.156	5,935	2,697		8	946
F	350,500	0.156	5,958	2,695		9	946
G	457,500	0.157	5,974	2,566	94	13	946
<b>Emergency scenario</b>							
<i>Solutions</i>	<i>Initial investment</i> [\$]	<i>COE</i> [\$]	<i>NPC</i> [\$]	<i>Electricity purchased</i> [kWh]	<i>Biogas</i> [kg/year]	<i>Renewable fraction</i> [%]	<i>Excess electricity</i> [kWh]
A	352,500	0.099	3,778	2,945	94	13	964.4
B	372,500	0.100	3,799	2,563	94	13	964.4
C	22,500	0.102	3,892	2,814	94	3	
D	456,000	0.105	4,003	2,567	94	13	1,646
E	476,000	0.106	4,024	2,564	94	13	1,646
<b>“Selling electricity back” scenario</b>							
<i>Solutions</i>	<i>Initial investment</i> [\$]	<i>COE</i> [\$]	<i>NPC</i> [\$]	<i>Electricity purchased</i> [kWh]	<i>Biogas</i> [kg/year]	<i>Renewable fraction</i> [%]	<i>Excess electricity</i> [kWh]
A	0	0.040	1,523	2,945			
B	7,500	0.040	1,527	2,902	31	1	
C	14,000	0.040	1,533	2,935		0.4	

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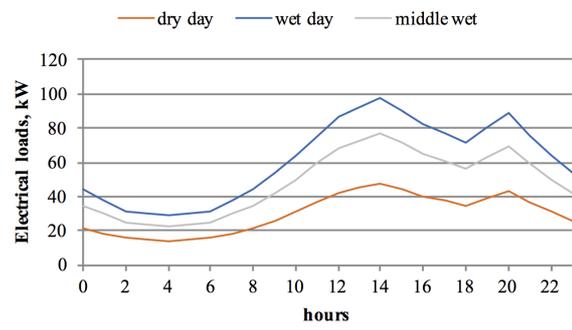
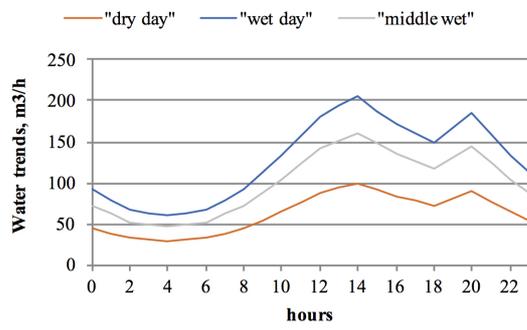
1032 Figure 1



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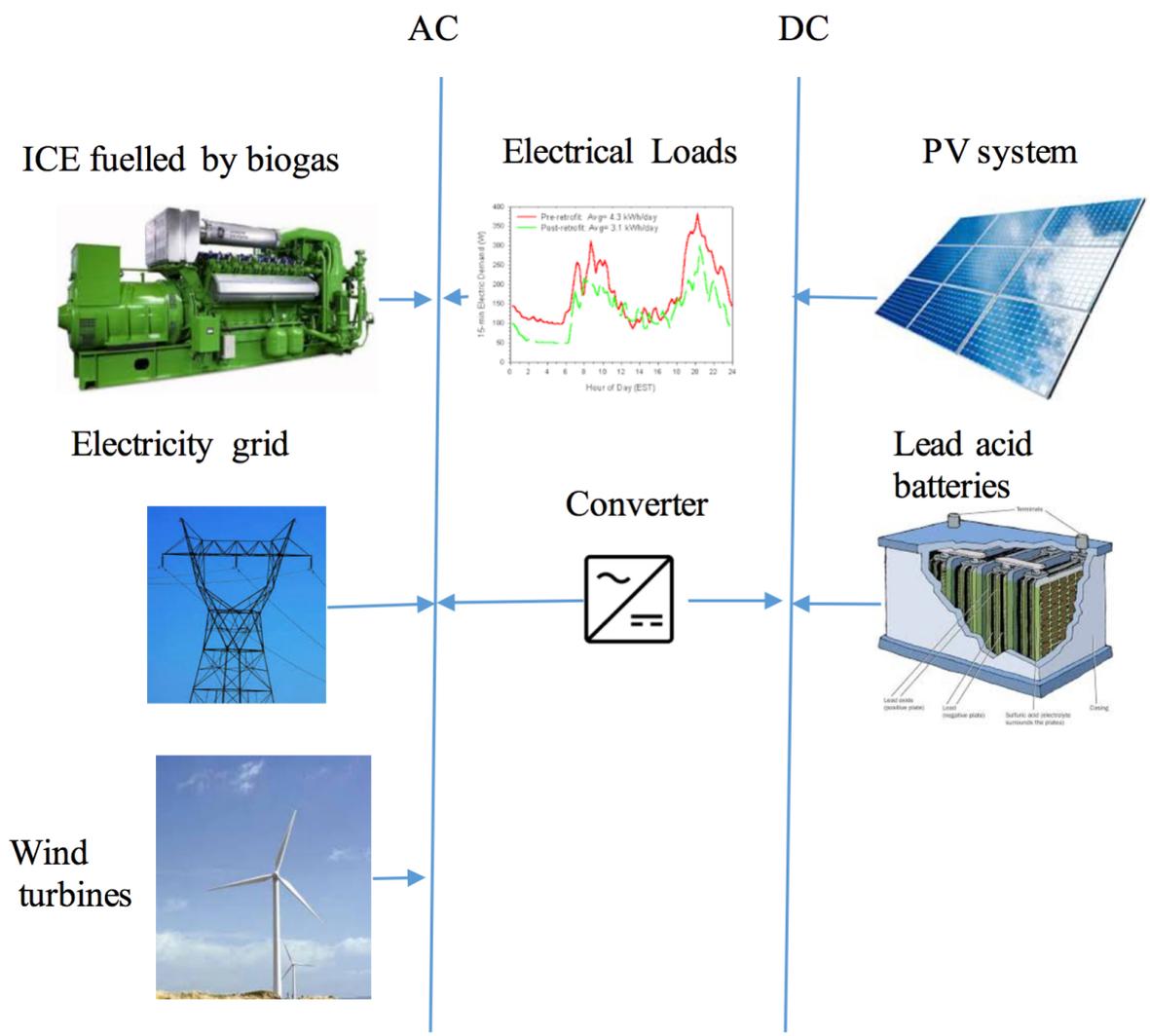
1035 Figure 2



1036 a)

b)

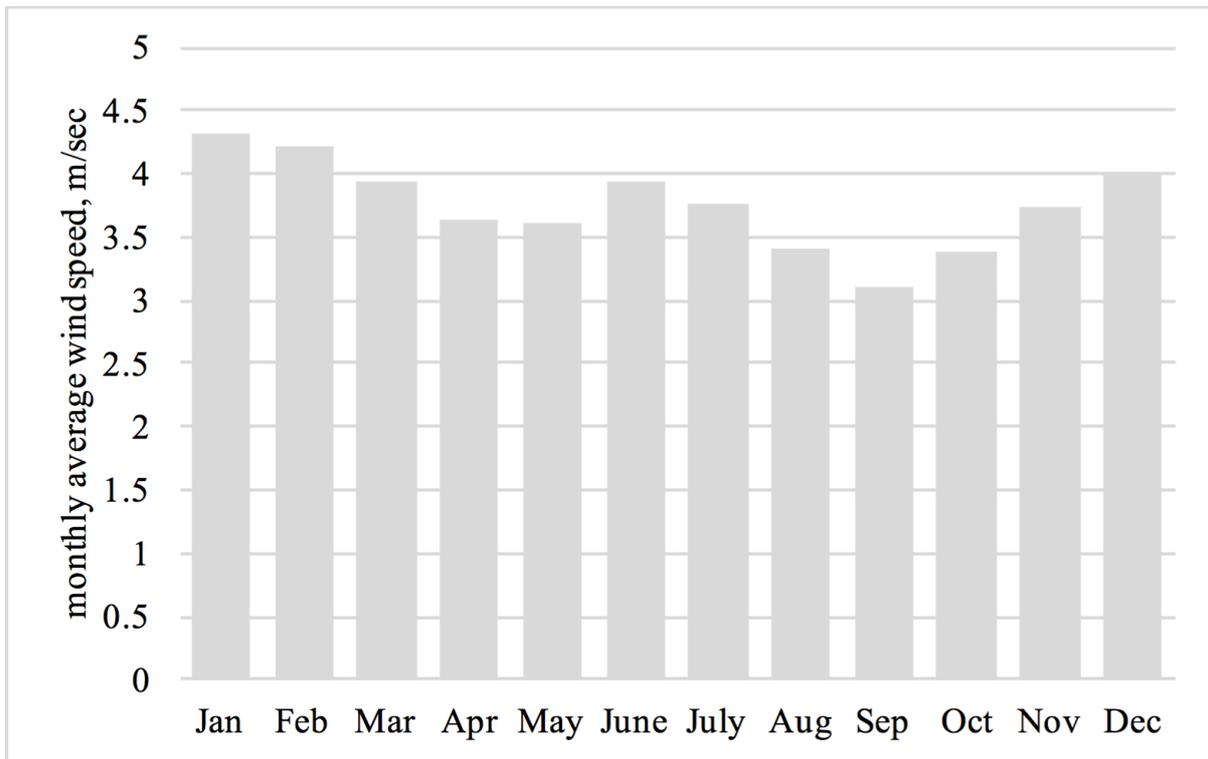
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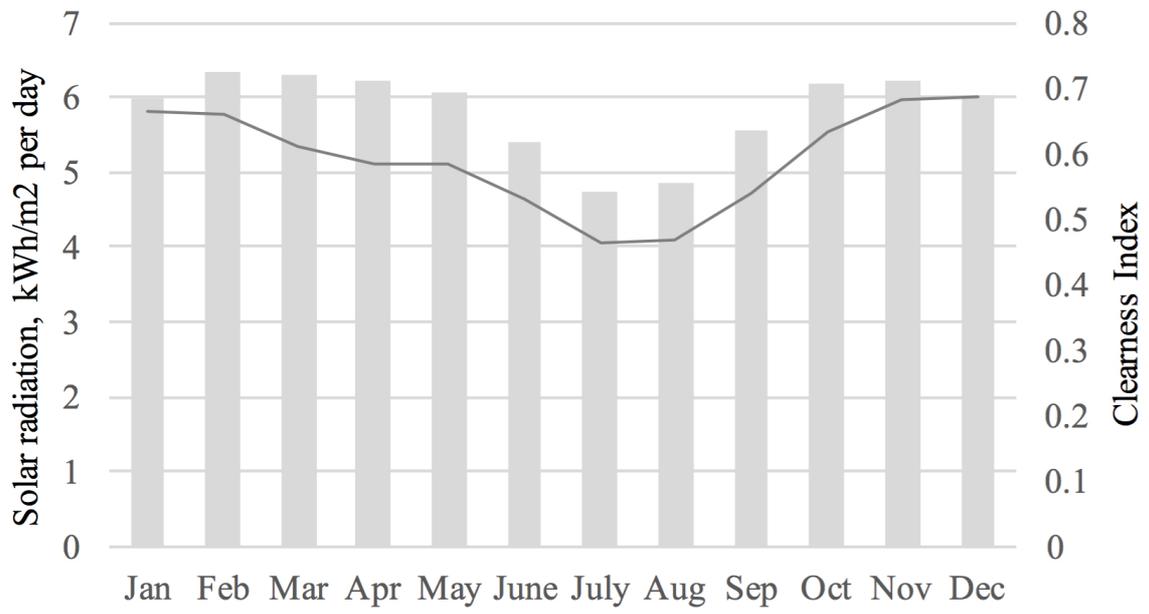
1041 Figure 4



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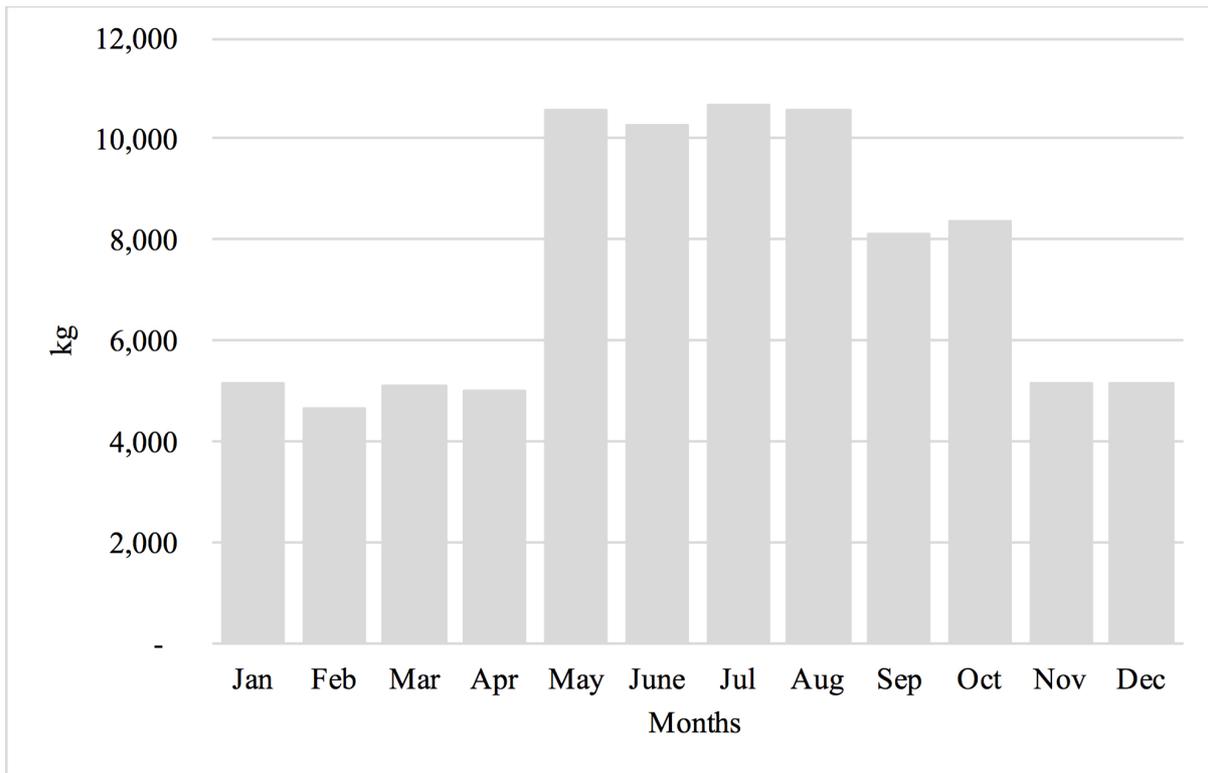
1044 Figure 5



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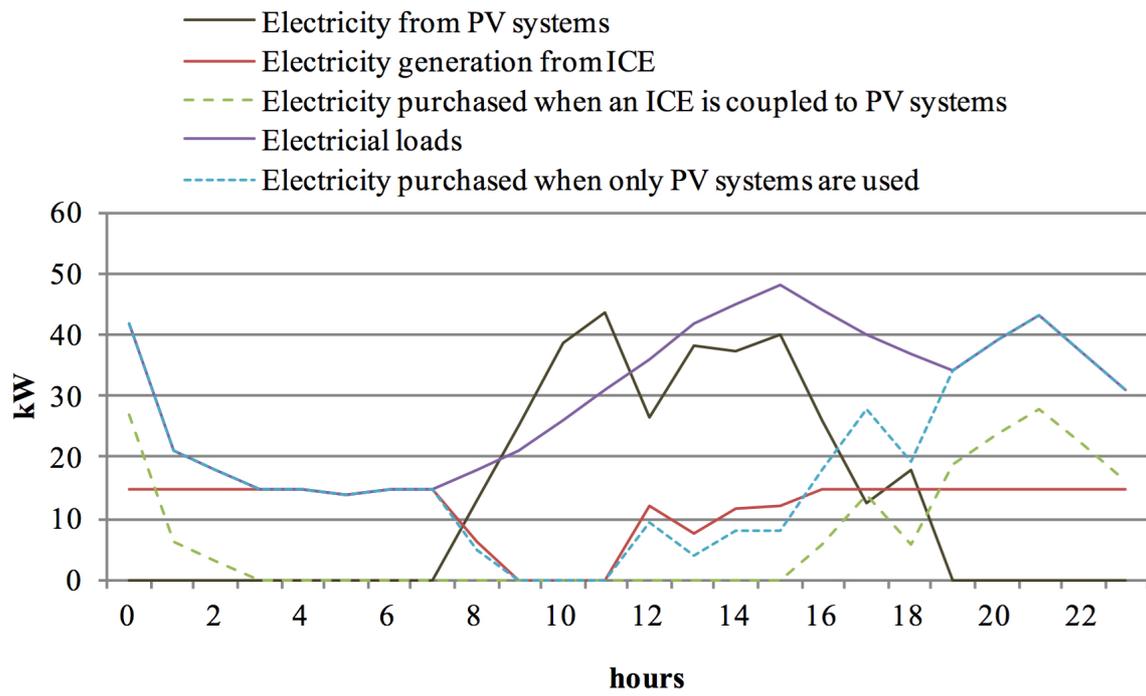
1047 Figure 6



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1050 Figure 7



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